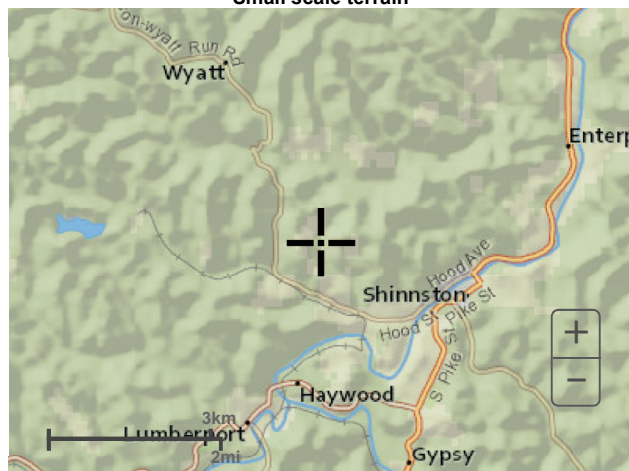
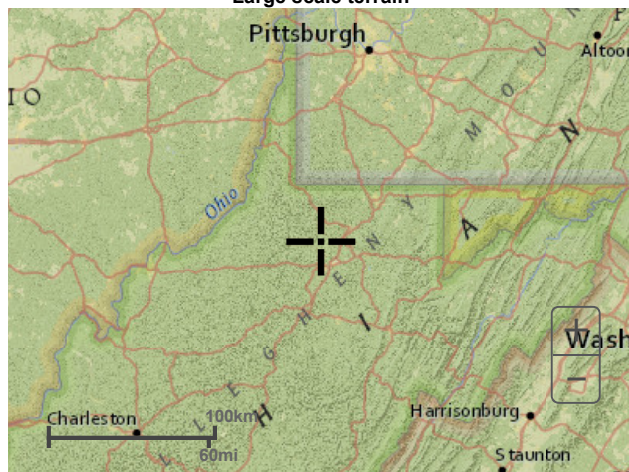


## Maps & aerals

Small scale terrain



Large scale terrain



Large scale map



### Large scale aerial



[Back to Top](#)

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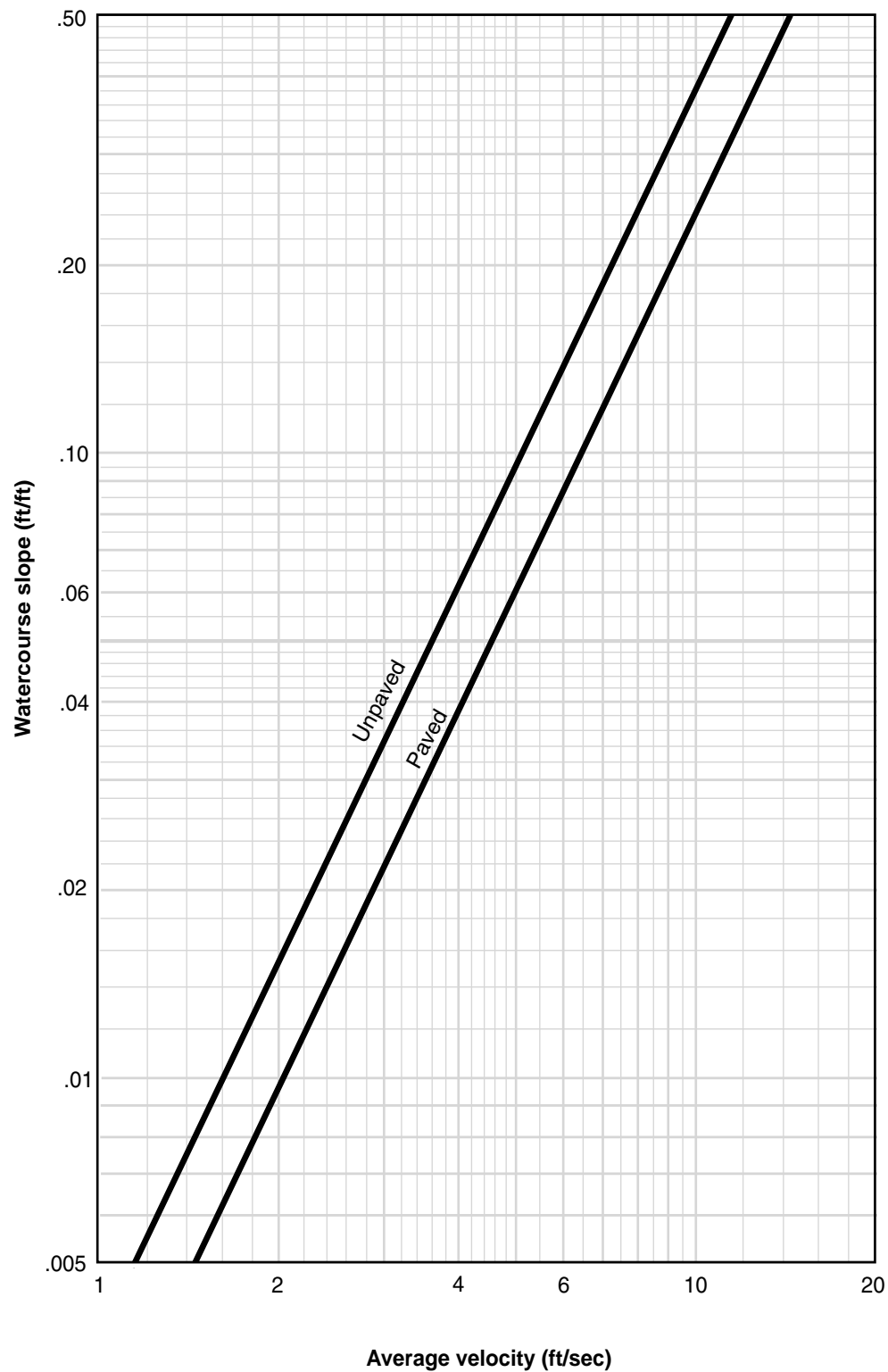
[US Department of Commerce](#)  
[National Oceanic and Atmospheric Administration](#)  
[National Weather Service](#)  
[National Water Center](#)  
1325 East West Highway  
Silver Spring, MD 20910  
Questions?: [HDSC.Questions@noaa.gov](mailto:HDSC.Questions@noaa.gov)

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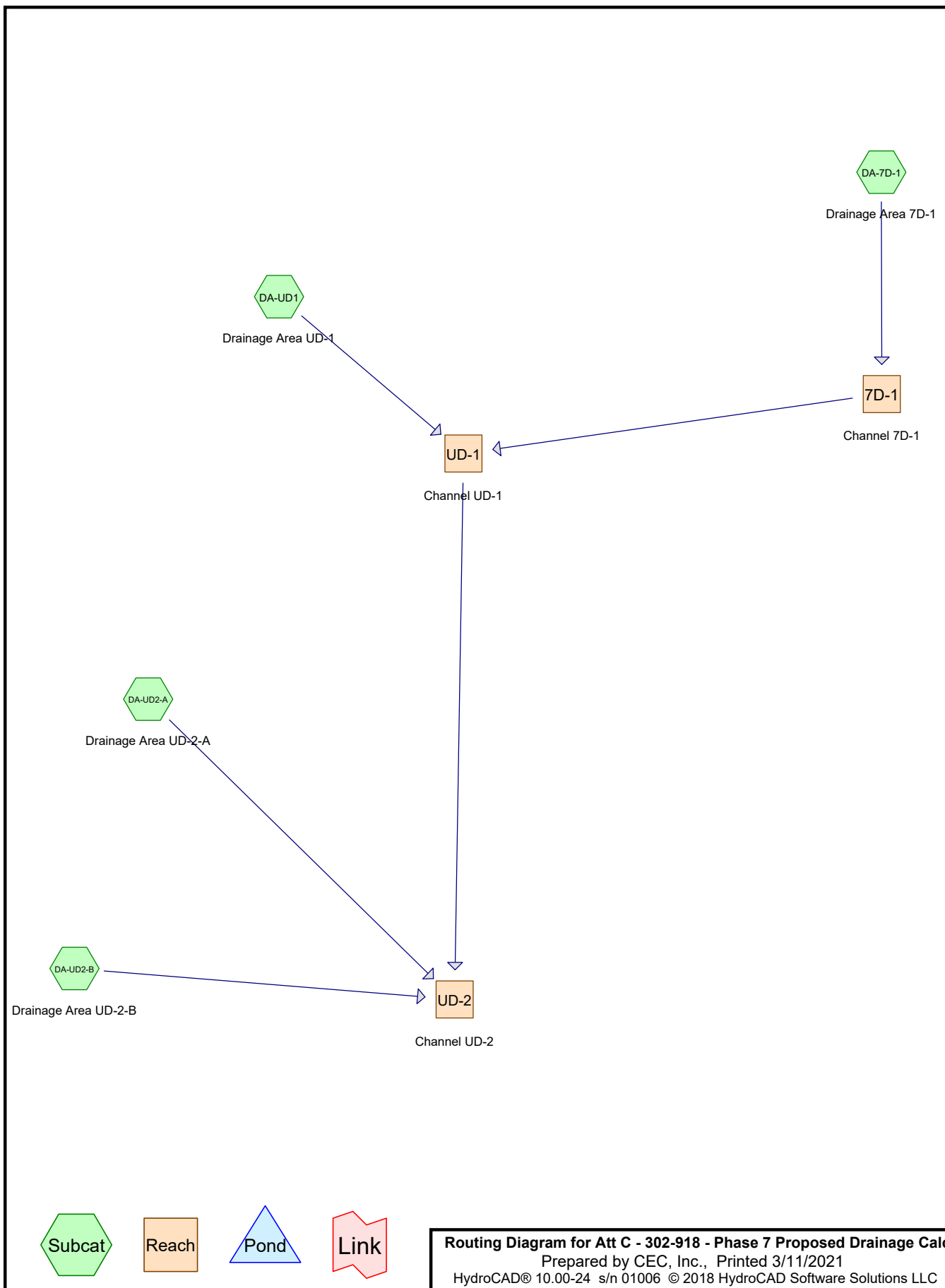


**ATTACHMENT B**

**TR-55 FIGURE 3-1**

**Figure 3-1** Average velocities for estimating travel time for shallow concentrated flow

**ATTACHMENT C**  
**HYDROCAD OUTPUT FILES**





## Att C - 302-918 - Phase 7 Proposed Drainage Calcs

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Page 2

### Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
24.100	70	Existing fields/undisturbed woods (DA-7D-1, DA-UD1, DA-UD2-A, DA-UD2-B)
<b>24.100</b>	<b>70</b>	<b>TOTAL AREA</b>

**Att C - 302-918 - Phase 7 Proposed Drainage Calcs**

Prepared by CEC, Inc.

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Page 3

**Soil Listing (all nodes)**

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
0.000	HSG C	
0.000	HSG D	
24.100	Other	DA-7D-1, DA-UD1, DA-UD2-A, DA-UD2-B
<b>24.100</b>		<b>TOTAL AREA</b>

**Att C - 302-918 - Phase 7 Proposed Drainage Calcs**

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**Ground Covers (all nodes)**

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchmen Numbers
0.000	0.000	0.000	0.000	24.100	24.100	Existing fields/undisturbed woods	
<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>24.100</b>	<b>24.100</b>	<b>TOTAL AREA</b>	

Time span=1.00-96.00 hrs, dt=0.05 hrs, 1901 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**SubcatchmentDA-7D-1: Drainage Area 7D-1** Runoff Area=2.500 ac 0.00% Impervious Runoff Depth=1.40"  
 Flow Length=422' Tc=14.2 min CN=70 Runoff=4.47 cfs 0.291 af

**SubcatchmentDA-UD1: Drainage Area UD-1** Runoff Area=2.800 ac 0.00% Impervious Runoff Depth=1.40"  
 Flow Length=665' Tc=18.3 min CN=70 Runoff=4.37 cfs 0.326 af

**SubcatchmentDA-UD2-A: Drainage Area** Runoff Area=2.200 ac 0.00% Impervious Runoff Depth=1.40"  
 Flow Length=455' Tc=11.8 min CN=70 Runoff=4.29 cfs 0.256 af

**SubcatchmentDA-UD2-B: Drainage Area** Runoff Area=16.600 ac 0.00% Impervious Runoff Depth=1.40"  
 Flow Length=590' Tc=11.8 min CN=70 Runoff=32.40 cfs 1.932 af

**Reach 7D-1: Channel 7D-1** Avg. Flow Depth=0.56' Max Vel=4.74 fps Inflow=4.47 cfs 0.291 af  
 n=0.045 L=680.0' S=0.1015 '/' Capacity=16.63 cfs Outflow=4.25 cfs 0.291 af

**Reach UD-1: Channel UD-1** Avg. Flow Depth=0.59' Max Vel=6.41 fps Inflow=8.56 cfs 0.617 af  
 n=0.015 L=900.0' S=0.0167 '/' Capacity=64.93 cfs Outflow=8.26 cfs 0.617 af

**Reach UD-2: Channel UD-2** Avg. Flow Depth=0.90' Max Vel=11.86 fps Inflow=40.84 cfs 2.805 af  
 n=0.015 L=3,840.0' S=0.0328 '/' Capacity=204.34 cfs Outflow=35.15 cfs 2.805 af

**Total Runoff Area = 24.100 ac Runoff Volume = 2.805 af Average Runoff Depth = 1.40"**  
**100.00% Pervious = 24.100 ac 0.00% Impervious = 0.000 ac**



### Summary for Subcatchment DA-7D-1: Drainage Area 7D-1

Runoff = 4.47 cfs @ 12.07 hrs, Volume= 0.291 af, Depth= 1.40"

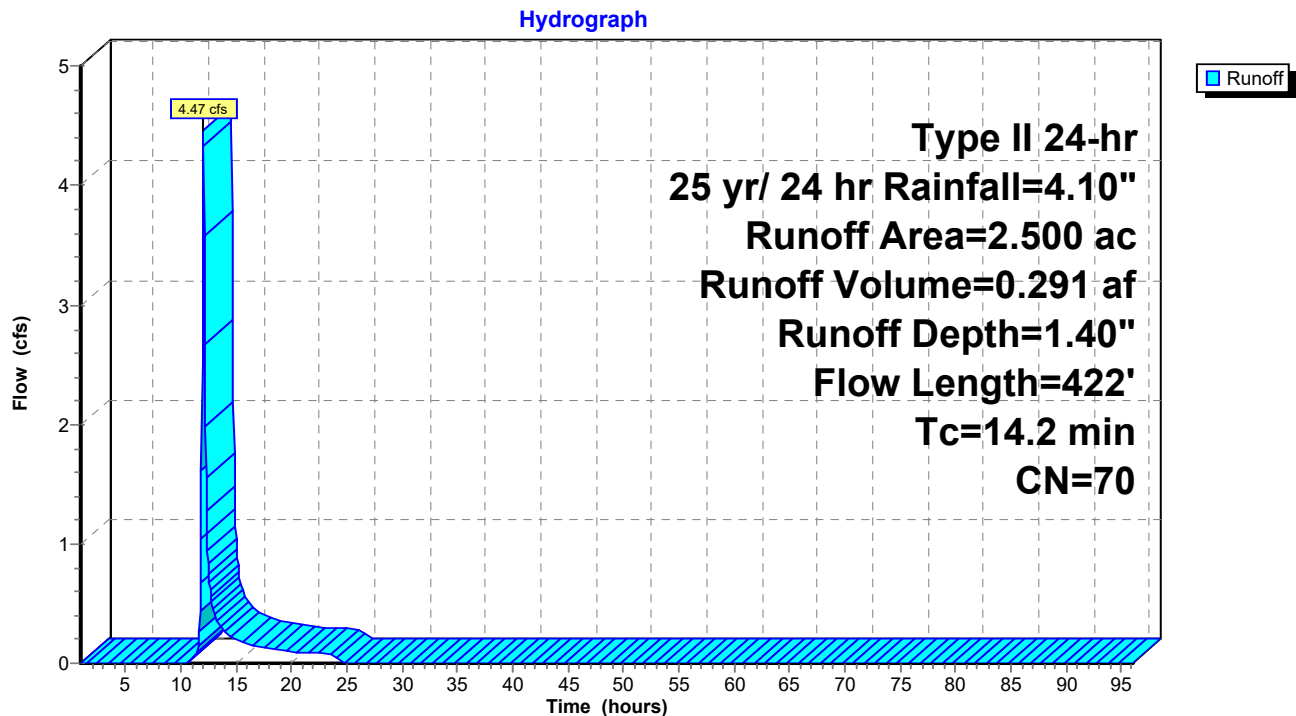
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-96.00 hrs, dt= 0.05 hrs  
 Type II 24-hr 25 yr/ 24 hr Rainfall=4.10"

Area (ac)	CN	Description
* 2.500	70	Existing fields/undisturbed woods
2.500		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.3	100	0.0900	0.13		<b>Sheet Flow, Sheet</b>
					Woods: Light underbrush n= 0.400 P2= 2.52"
0.7	202	0.1000	5.09		<b>Shallow Concentrated Flow, Shallow 1</b>
					Unpaved Kv= 16.1 fps
0.2	120	0.3500	9.52		<b>Shallow Concentrated Flow, Shallow 2</b>
					Unpaved Kv= 16.1 fps
14.2	422	Total			

### Subcatchment DA-7D-1: Drainage Area 7D-1



### Summary for Subcatchment DA-UD1: Drainage Area UD-1

Runoff = 4.37 cfs @ 12.12 hrs, Volume= 0.326 af, Depth= 1.40"

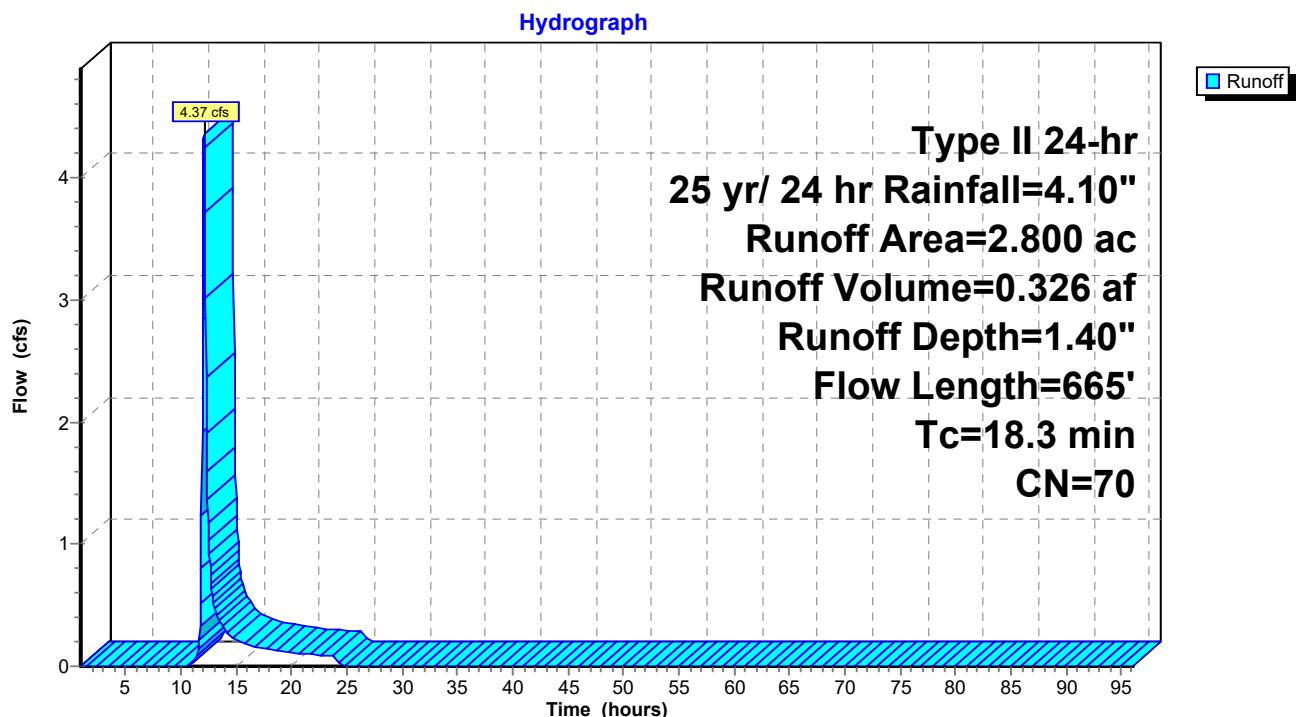
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-96.00 hrs, dt= 0.05 hrs  
 Type II 24-hr 25 yr/ 24 hr Rainfall=4.10"

Area (ac)	CN	Description
* 2.800	70	Existing fields/undisturbed woods
2.800		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
15.6	100	0.0600	0.11		<b>Sheet Flow, Sheet</b> Woods: Light underbrush n= 0.400 P2= 2.52"
2.6	500	0.0400	3.22		<b>Shallow Concentrated Flow, Shallow 1</b> Unpaved Kv= 16.1 fps
0.1	65	0.2500	8.05		<b>Shallow Concentrated Flow, Shallow 2</b> Unpaved Kv= 16.1 fps
18.3	665	Total			

### Subcatchment DA-UD1: Drainage Area UD-1



### Summary for Subcatchment DA-UD2-A: Drainage Area UD-2-A

Runoff = 4.29 cfs @ 12.05 hrs, Volume= 0.256 af, Depth= 1.40"

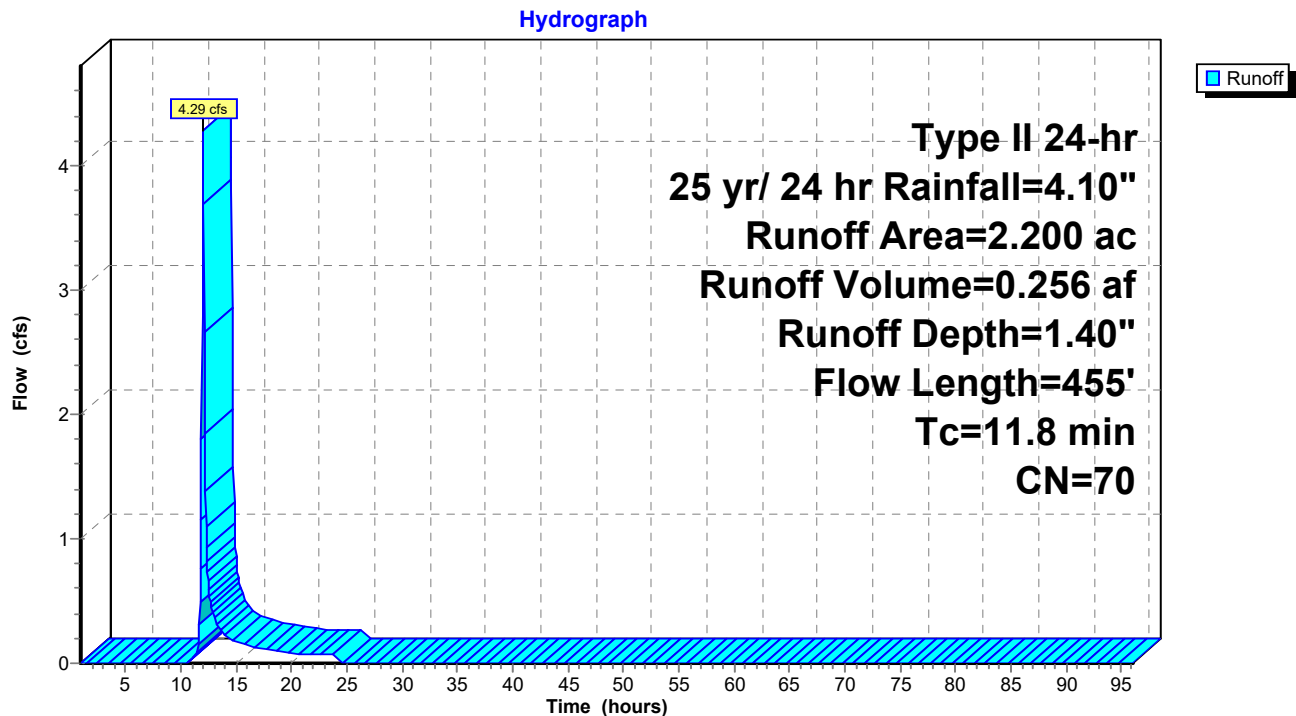
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-96.00 hrs, dt= 0.05 hrs  
 Type II 24-hr 25 yr/ 24 hr Rainfall=4.10"

Area (ac)	CN	Description
* 2.200	70	Existing fields/undisturbed woods
2.200		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.1	100	0.1400	0.15		<b>Sheet Flow, Sheet</b> Woods: Light underbrush n= 0.400 P2= 2.52"
0.5	245	0.2500	8.05		<b>Shallow Concentrated Flow, Shallow 1</b> Unpaved Kv= 16.1 fps
0.2	110	0.3200	9.11		<b>Shallow Concentrated Flow, Shallow 2</b> Unpaved Kv= 16.1 fps
11.8	455	Total			

### Subcatchment DA-UD2-A: Drainage Area UD-2-A



### Summary for Subcatchment DA-UD2-B: Drainage Area UD-2-B

Runoff = 32.40 cfs @ 12.05 hrs, Volume= 1.932 af, Depth= 1.40"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-96.00 hrs, dt= 0.05 hrs  
 Type II 24-hr 25 yr/ 24 hr Rainfall=4.10"

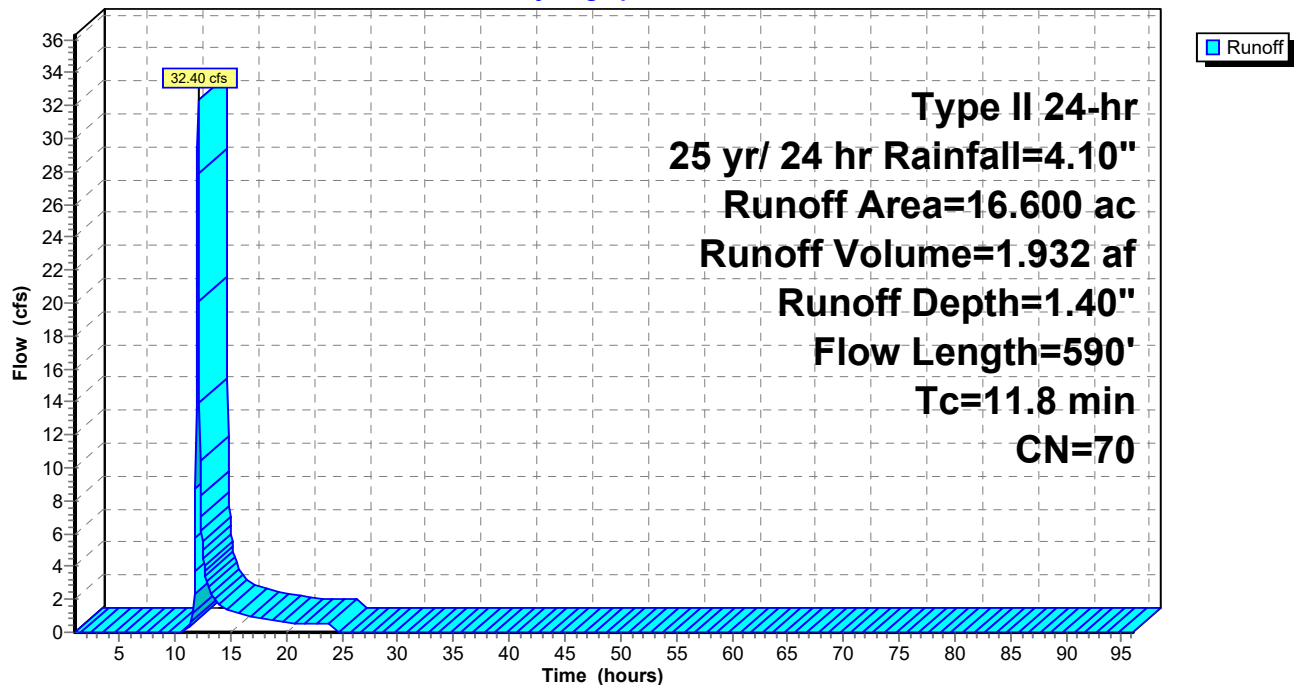
Area (ac)	CN	Description
* 16.600	70	Existing fields/undisturbed woods
16.600		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.5	100	0.1600	0.16		<b>Sheet Flow, Sheet</b>
					Woods: Light underbrush n= 0.400 P2= 2.52"
1.3	490	0.1500	6.24		<b>Shallow Concentrated Flow, Shallow 1</b>
					Unpaved Kv= 16.1 fps
11.8	590	Total			

### Subcatchment DA-UD2-B: Drainage Area UD-2-B

Hydrograph





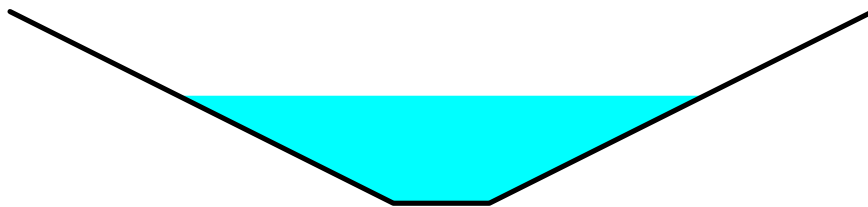
### Summary for Reach 7D-1: Channel 7D-1

Inflow Area = 2.500 ac, 0.00% Impervious, Inflow Depth = 1.40" for 25 yr/ 24 hr event  
 Inflow = 4.47 cfs @ 12.07 hrs, Volume= 0.291 af  
 Outflow = 4.25 cfs @ 12.15 hrs, Volume= 0.291 af, Atten= 5%, Lag= 4.4 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-96.00 hrs, dt= 0.05 hrs  
 Max. Velocity= 4.74 fps, Min. Travel Time= 2.4 min  
 Avg. Velocity = 1.75 fps, Avg. Travel Time= 6.5 min

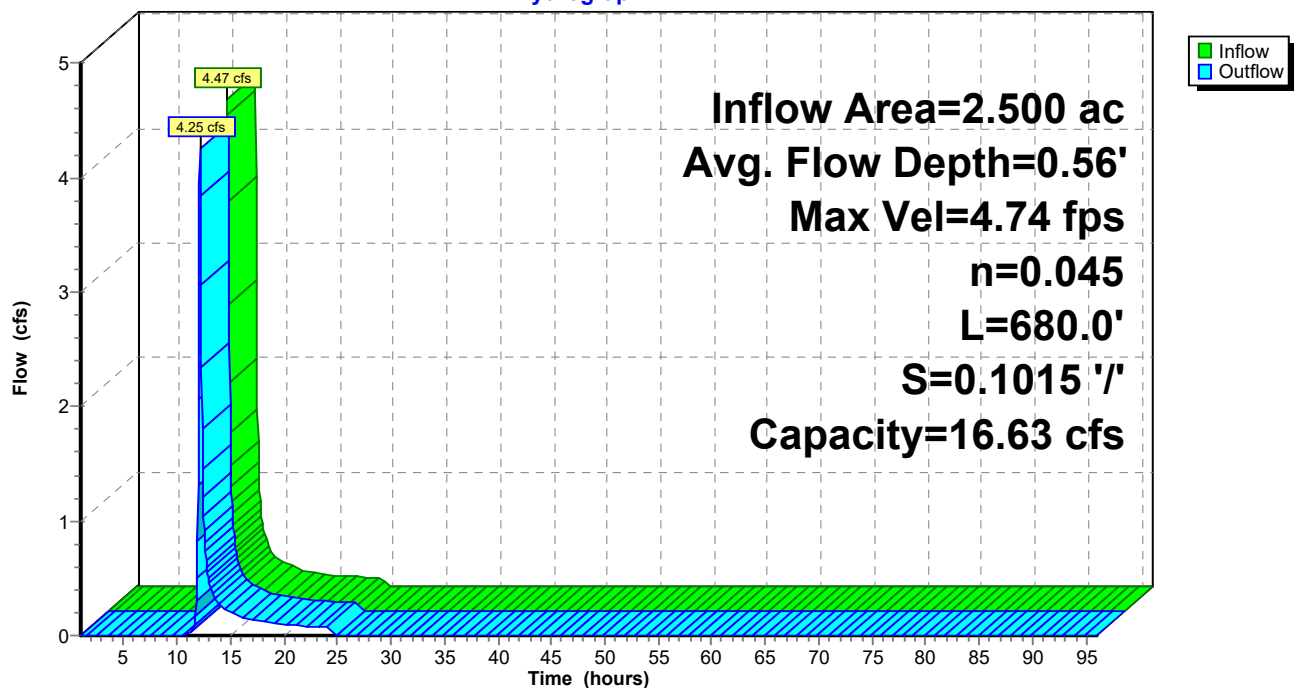
Peak Storage= 619 cf @ 12.10 hrs  
 Average Depth at Peak Storage= 0.56'  
 Bank-Full Depth= 1.00' Flow Area= 2.5 sf, Capacity= 16.63 cfs

0.50' x 1.00' deep channel, n= 0.045 Vegetated  
 Side Slope Z-value= 2.0 '/' Top Width= 4.50'  
 Length= 680.0' Slope= 0.1015 '/'  
 Inlet Invert= 1,414.00', Outlet Invert= 1,345.00'



Reach 7D-1: Channel 7D-1

Hydrograph



### Summary for Reach UD-1: Channel UD-1

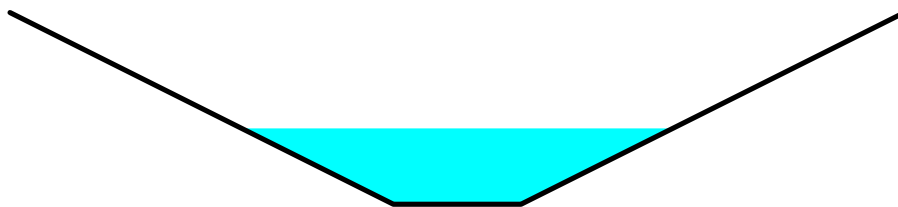
[62] Hint: Exceeded Reach 7D-1 OUTLET depth by 0.11' @ 12.25 hrs

Inflow Area = 5.300 ac, 0.00% Impervious, Inflow Depth = 1.40" for 25 yr/ 24 hr event  
 Inflow = 8.56 cfs @ 12.13 hrs, Volume= 0.617 af  
 Outflow = 8.26 cfs @ 12.21 hrs, Volume= 0.617 af, Atten= 4%, Lag= 4.2 min

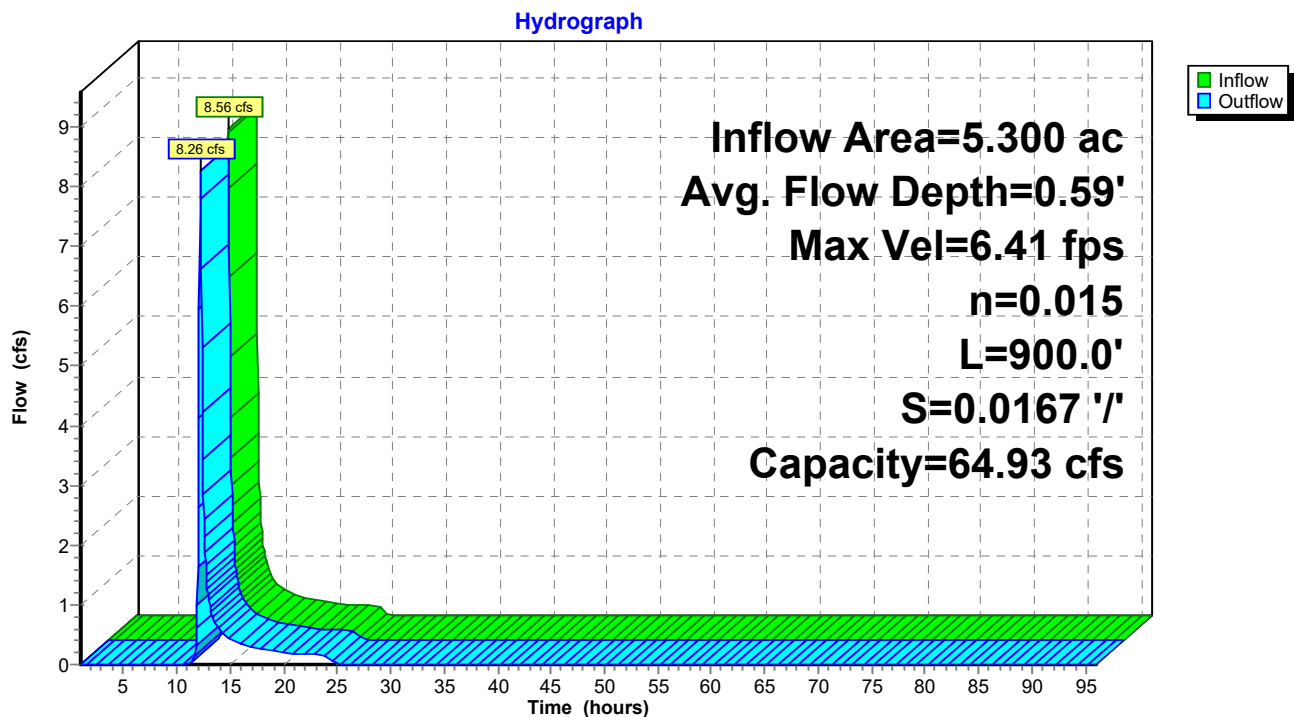
Routing by Stor-Ind+Trans method, Time Span= 1.00-96.00 hrs, dt= 0.05 hrs  
 Max. Velocity= 6.41 fps, Min. Travel Time= 2.3 min  
 Avg. Velocity = 2.26 fps, Avg. Travel Time= 6.6 min

Peak Storage= 1,172 cf @ 12.16 hrs  
 Average Depth at Peak Storage= 0.59'  
 Bank-Full Depth= 1.50' Flow Area= 6.0 sf, Capacity= 64.93 cfs

1.00' x 1.50' deep channel, n= 0.015 Concrete  
 Side Slope Z-value= 2.0 '/' Top Width= 7.00'  
 Length= 900.0' Slope= 0.0167 '/'  
 Inlet Invert= 1,345.00', Outlet Invert= 1,330.00'



Reach UD-1: Channel UD-1



## Summary for Reach UD-2: Channel UD-2

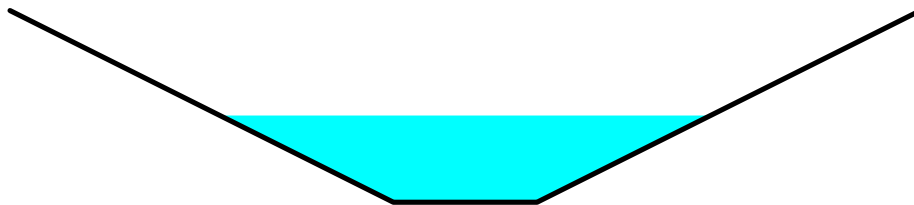
[62] Hint: Exceeded Reach UD-1 OUTLET depth by 0.35' @ 12.05 hrs

Inflow Area = 24.100 ac, 0.00% Impervious, Inflow Depth = 1.40" for 25 yr/ 24 hr event  
 Inflow = 40.84 cfs @ 12.06 hrs, Volume= 2.805 af  
 Outflow = 35.15 cfs @ 12.21 hrs, Volume= 2.805 af, Atten= 14%, Lag= 9.4 min

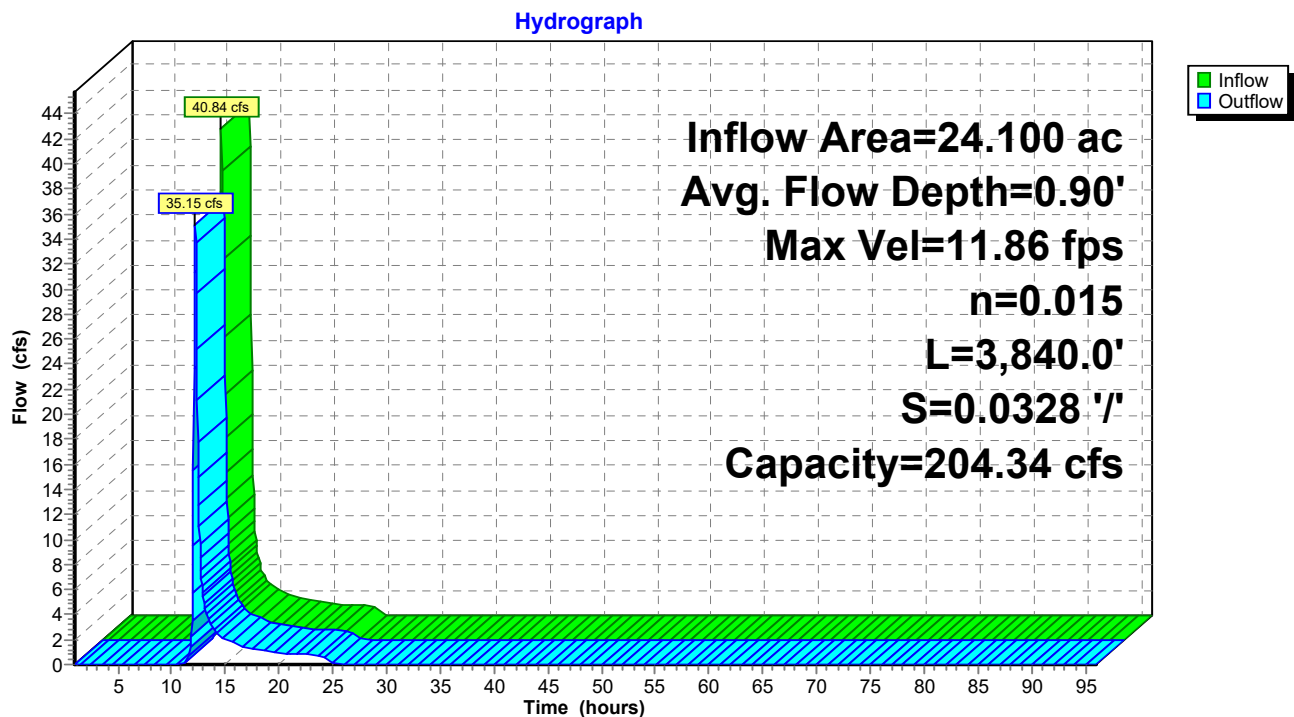
Routing by Stor-Ind+Trans method, Time Span= 1.00-96.00 hrs, dt= 0.05 hrs  
 Max. Velocity= 11.86 fps, Min. Travel Time= 5.4 min  
 Avg. Velocity = 3.78 fps, Avg. Travel Time= 17.0 min

Peak Storage= 11,475 cf @ 12.12 hrs  
 Average Depth at Peak Storage= 0.90'  
 Bank-Full Depth= 2.00' Flow Area= 11.0 sf, Capacity= 204.34 cfs

1.50' x 2.00' deep channel, n= 0.015 Concrete  
 Side Slope Z-value= 2.0 '/' Top Width= 9.50'  
 Length= 3,840.0' Slope= 0.0328 '/'  
 Inlet Invert= 1,330.00', Outlet Invert= 1,204.00'



Reach UD-2: Channel UD-2



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**APPENDIX E**  
**LINER SYSTEM CALCULATIONS**

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## **ANCHOR TRENCH**

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Civil & Environmental Consultants, Inc.

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SUBJECT	<b>Anchor Trench Design</b>	PROJECT NO.	<b>302-918.0030</b>
PROJECT	<b>Phase 7 CCB Landfill Expansion</b>	PAGE	<b>1</b> OF <b>3</b>
<b>Harrison Power Station</b>			
MADE BY	<b>AAW</b>	DATE	<b>12/16/2020</b>
CHECKED BY	<b>TJK</b>	DATE	<b>3/12/2021</b>

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## OBJECTIVE

Analyze the proposed anchor trench design for the Phase 7 expansion to determine if it provides adequate short term pull-out resistance for the proposed 3.0H:1V baseliner slope.

The West Virginia Title 33 Legislative Rule Series 1 (§33-1) requires that the geomembrane;

*4.5.d.5.B.9 Be designed to withstand the calculated tensile forces acting upon the synthetic materials when installed on slopes greater than twenty-five percent (25%);*

and

*4.5.d.5.B.9 Be anchored a minimum of twenty-four (24) inches horizontally back from the edge of the top of the slope. The liner must be anchored by cutting a trench twelve (12) to sixteen (16) inches in depth, laying the liner across the soil perimeter of the trench, backfilling the trench, and compacting the backfill material.*

A separate anchor trench calculation was performed by GAI for the Phase 6A proposed 3H:1V baseliner slopes and includes an anchor trench design the a 3-foot long berm runout and a 1-foot long anchor runout.

## REFERENCES

1. Koerner, Robert. Designing with Geosynthetics, Second Edition, Prentice Hall, 1990.
2. Harrison Power Station, Phase 6A Expansion Area, Bottom Liner Anchor Trench Design Calculations, GAI Consultants, 2017

## ALLOWABLE STRENGTH

The allowable short-term pull-out resistance is based on the maximum linear tension of the proposed geosynthetic liner. From GRI GM 13, 60-mil HDPE textured geomembrane liner should have a minimum yield strength of 126 lbs/inch and minimum break strength of 90 lbs/inch.

$$T_{\text{allow}} = (126 \text{ lb/in})/2.5 = 50.4 \text{ lb/in} = 605 \text{ lb/ft}$$



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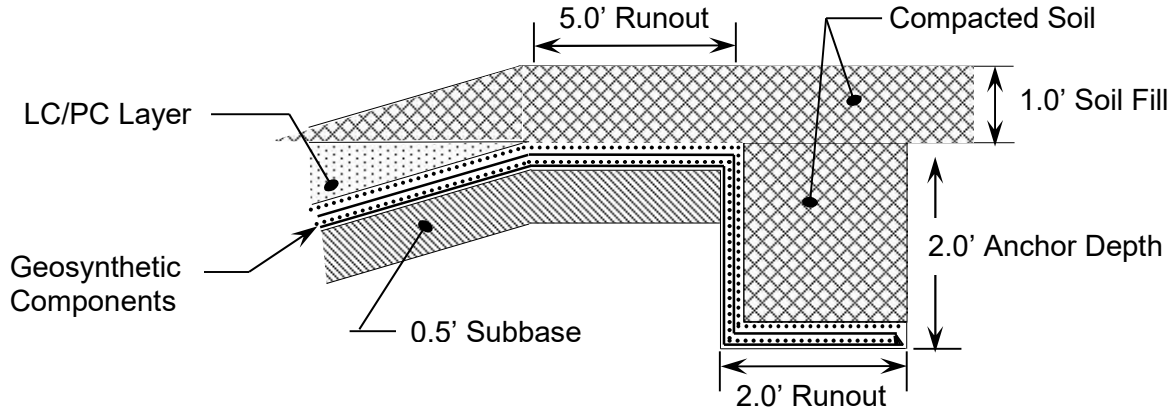
SUBJECT	<b>Anchor Trench Design</b>	PROJECT NO.	<b>302-918.0030</b>
PROJECT	<b>Phase 7 CCB Landfill Expansion</b>	PAGE	<b>2</b> OF <b>3</b>
<b>Harrison Power Station</b>			
MADE BY	<b>AAW</b>	DATE	<b>12/16/2020</b>
CHECKED BY	<b>TJK</b>	DATE	<b>3/12/2021</b>

## ANALYSIS

The proposed Phase 7 liner and leachate collection system consists of the following components (from bottom to top):

1. 6-inch thick Subbase Layer;
2. Double Sided Geocomposite Drainage Net (GDN) Leachate Detection Zone;
3. Geosynthetic Clay Liner (GCL);
4. 60-mil HDPE Textured Geomembrane Liner;
5. 16 oz/sy Cushion Geotextile;
6. 12-inch thick Leachate Collection Zone consisting of Granular Bottom Ash material (or sand); and
7. 12-inch thick Protective Cover Layer consisting of CCB material.

The proposed anchor trench design is shown below:



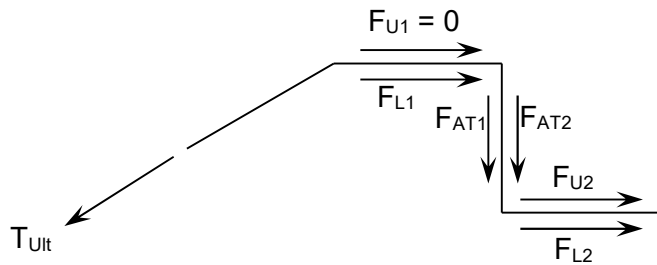
- $d_{sc} = 1.0'$  (soil fill depth)  
 $\gamma_{sc} = 120$  pcf (cover soil unit weight)  
 $\phi_{SB} = 25.5^\circ$  (subbase soil internal friction angle)  
 $\gamma_{SB} = 115$  pcf (subbase soil unit weight)  
 $\delta_1 = 18.4^\circ$  (slope angle beneath the geomembrane, 3.0H:1V)  
 $\delta_2 = 27^\circ$  (interface friction angle)  
 $L_{RO1} = 5.0'$  (berm runout)  
 $L_{RO2} = 2.0'$  (trench runout)  
 $d_{AT} = 2.0'$  (trench depth)  
 $d_{AT'} = 3.0'$  (effective depth)



# Civil & Environmental Consultants, Inc.

SUBJECT	<b>Anchor Trench Design</b>	PROJECT NO.	<b>302-918.0030</b>
PROJECT	<b>Phase 7 CCB Landfill Expansion</b>	PAGE	<b>3</b> OF <b>3</b>
<b>Harrison Power Station</b>			
MADE BY	<b>AAW</b>	DATE	<b>12/16/2020</b>
CHECKED BY	<b>TJK</b>	DATE	<b>3/12/2021</b>

The frictional resistance mobilized by the anchor trench geometry shown above is resolved as follows:



$$\begin{aligned}
 F_{L1} &= \gamma_{SC} d_{SC} \tan \delta_1 L_{RO1} \\
 F_{AT1} &= (1 - \sin \phi_{SB}) \gamma_{SB} H_{Avg} \tan \delta_1 d_{AT} \\
 F_{AT2} &= (1 - \sin \phi_{SB}) \gamma_{SB} H_{Avg} \tan \delta_2 d_{AT} \\
 F_{U1} &= 0 \text{ (soil will crack and move with the liner)} \\
 F_{U2} &= \gamma_{SC} d_{AT} \tan \delta_2 L_{RO2} \\
 F_{L2} &= \gamma_{SC} d_{AT} \tan \delta_1 L_{RO2}
 \end{aligned}$$

$$H_{Avg} = \text{Average Anchor Trench Depth} = (2' + 1')/2 = 1.5 \text{ feet}$$

Thus, for static equilibrium conditions:

$$T_{Ult} = F_{L1} + F_{AT1} + F_{AT2} + F_{U2} + F_{L2}$$

$$\begin{aligned}
 &= \gamma_{SC} d_{SC} \tan \delta_1 L_{RO1} \\
 &+ (1 - \sin \phi_{SB}) \gamma_{SB} H_{Avg} \tan \delta_1 d_{AT} \\
 &+ (1 - \sin \phi_{SB}) \gamma_{SB} H_{Avg} \tan \delta_2 d_{AT} \\
 &+ 0 \\
 &+ \gamma_{SC} d_{AT} \tan \delta_2 L_{RO2} \\
 &+ \gamma_{SC} d_{AT} \tan \delta_1 L_{RO2} \\
 &= (120 \text{ pcf} * 1.0' * \tan 18.4^\circ * 5.0') \\
 &+ [(1 - \sin 25.5^\circ) * 115 \text{ pcf} * 1.5' * \tan 18.4^\circ * 2.0'] \\
 &+ [(1 - \sin 25.5^\circ) * 115 \text{ pcf} * 1.5' * \tan 27^\circ * 2.0'] \\
 &+ (120 \text{ pcf} * 3.0' * \tan 27^\circ * 2.0') \\
 &+ (120 \text{ pcf} * 3.0' * \tan 18.4^\circ * 2.0')
 \end{aligned}$$

$$= 200 \text{ lb/ft} + 65 \text{ lb/ft} + 100 \text{ lb/ft} + 367 \text{ lb/ft} + 240 \text{ lb/ft} = 972 \text{ lb/ft}$$

$$\begin{aligned}
 T_{allow} &\leq T_{Ult} \\
 605 \text{ ppf} &\leq 972 \text{ ppf} \quad \underline{\text{OK}}
 \end{aligned}$$

## CONCLUSION

The proposed anchor trench will provide sufficient frictional resistance to avoid pull-out at an applied force of 972 lb/ft for the proposed liner system.



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## **PERMEABILITY EQUIVALENCY CALCULATION - GDN**

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Civil & Environmental Consultants, Inc.

SUBJECT **Baseliner Leachate Detection Zone Geocomposite  
Transmissivity**

PROJECT NO. **302-918**

PROJECT **Phase 7 CCB Landfill Expansion**

PAGE **1** OF **4**

**Harrison Power Station**

MADE BY **AAW** DATE **12/16/2020** CHECKED BY **TJK** DATE **3/12/2021**

---

## OBJECTIVE

The objective of this analysis is to specify the transmissivity of the geocomposite for the landfill baseliner system. The West Virginia Title 33 Legislative Rule Series 1 (§33-1) requires in Rule 4.5.d.4 that the leachate detection zone must create a flow zone between the subbase and the composite liner system more permeable than  $1 \times 10^{-3}$  cm/sec. The leachate detection zone must be at least 12-inches thick.

## REFERENCES

1. Harrison Power Station, Phase 6A Expansion Area, Slope Stability Analysis, GAI Consultants, 2017
2. Harrison Power Station, Phase 6 Expansion Area, Slope Stability Analysis, GAI Consultants, 2015
3. Harrison Power Station, Phase 5 Expansion Area, Slope Stability Analysis, GAI Consultants, 2011
4. United States Environmental Protection Agency (USEPA), 2015. 40 CFR Parts 257 and 261 Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals from Electric Utilities; Final Rule. April 17, 2015.
5. USEPA, 1988. Guide to Technical Resources for the Design of Land Disposal Facilities. Document No. EPA/625/6-88-018. December 1988.
6. GRI Standard – GC8, Determination of the Allowable Flow Rate of a Drainage Geocomposite, January 9, 2013, Geosynthetic Research Institute (GRI).

## METHODOLOGY

### **GRI Standard – GC8, Determination of the Allowable Flow Rate of a Drainage Geocomposite**

This paper presents the methodology for application of reduction factors in the specification of required transmissivity of a geocomposite.

## PROPOSED BASELINER

The proposed Phase 7 liner and leachate collection system consists of the following components (from bottom to top):

- 6-inch thick Subbase Layer;
- Double Sided Geocomposite Drainage Net (GDN) Leachate Detection Zone;



## Civil & Environmental Consultants, Inc.

SUBJECT	<b>Baseliner Leachate Detection Zone Geocomposite Transmissivity</b>	PROJECT NO.	<b>302-918</b>
PROJECT	<b>Phase 7 CCB Landfill Expansion</b>	PAGE	<b>2</b> OF <b>4</b>
<b>Harrison Power Station</b>			
MADE BY	<b>AAW</b>	DATE	<b>12/16/2020</b>
CHECKED BY	<b>TJK</b>	DATE	<b>3/12/2021</b>

- Geosynthetic Clay Liner (GCL);
- 60-mil HDPE Textured Geomembrane Liner;
- 16 oz/sy Cushion Geotextile;
- 12-inch thick Leachate Collection Layer consisting of Granular Bottom Ash material (or sand); and
- 12-inch thick Protective Cover Layer consisting of CCB material.

### CALCULATIONS

#### Required Transmissivity

The West Virginia Title 33 Legislative Rule Series 1 (§33-1) requires in Rule 4.5.d.4 that the leachate detection zone have a minimum permeability of  $1 \times 10^{-3}$  cm/sec and have a minimum thickness of 12 inches. The required long term transmissivity is calculated as follows:

$$\theta_{lt} = k \cdot t$$

Where :

$\theta_{lt}$  = Long-term transmissivity of the drainage layer

k = Permeability of the drainage layer

t = Thickness of the drainage layer

$$\theta_{lt} = 1 \times 10^{-3} \frac{cm}{sec} (12 in) \left( 2.54 \frac{cm}{in} \right) \left( \frac{1 m^2}{10,000 cm^2} \right) = 3.048 \times 10^{-6} \frac{m^2}{sec}$$

Using the minimum leachate collection thickness and permeability, an equivalent long-term transmissivity of  $3.048 \times 10^{-6}$  m<sup>2</sup>/sec was calculated.

#### Specified Transmissivity

To meet this required long-term transmissivity, the specified value of transmissivity for the geocomposite at the time of testing must be higher than the long-term transmissivity to account for clogging and creep that will occur during long-term conditions.

From Koerner, 1998, "If the test setup does not model site specific conditions adequately, then adjustments to the laboratory value must be made." Since this transmissivity was determined for field conditions, the use of reduction factors is necessary. These reduction factors will be applied to calculate a transmissivity specification value to be used in laboratory quality assurance testing.



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Civil & Environmental Consultants, Inc.

SUBJECT	<b>Baseliner Leachate Detection Zone Geocomposite Transmissivity</b>	PROJECT NO.	<b>302-918</b>
PROJECT	<b>Phase 7 CCB Landfill Expansion</b>	PAGE	<b>3</b> OF <b>4</b>
<b>Harrison Power Station</b>			
MADE BY	<b>AAW</b>	DATE	<b>12/16/2020</b>
CHECKED BY	<b>TJK</b>	DATE	<b>3/12/2021</b>

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To account for the reduction in transmissivity over the long term, this transmissivity will be increased using reduction factors considering GRI Standard – GC8 to develop the transmissivity specification at the time of installation.

$$\text{Transmissivity}_{\text{act}} = \theta_{\text{lt}} * \text{FS}_D * (\text{RF}_{\text{IN}} * \text{RF}_{\text{CR}} * \text{RF}_{\text{CC}} * \text{RF}_{\text{BC}})$$

Where :

$\text{FS}_D$  = Overall factor of safety for drainage  
 $\text{RF}_{\text{IN}}$  = Reduction Factor for geotextile intrusion;  
 $\text{RF}_{\text{CR}}$  = Reduction Factor for creep deformation;  
 $\text{RF}_{\text{CC}}$  = Reduction Factor for chemical clogging (1.1 to 1.5); and  
 $\text{RF}_{\text{BC}}$  = Reduction Factor for biological clogging (1.1 to 1.3).

The reduction factors for the flow capacity of geocomposites having a geonet core used in landfill leachate detection zone are described below:

- The ultimate transmissivity ( $\theta_{\text{ult}}$ ) is calculated to achieve an overall drainage factor of safety of 2 ( $\text{FS}_D = 2$ ).
- Since the laboratory testing will be performed using site-specific boundary conditions, the reduction factor for intrusion of the geotextile into the geonet will be ignored ( $\text{RF}_{\text{IN}} = 1.0$ ).
- The reduction factor for creep was conservatively assumed for a total reduction factor of 20 ( $\text{RF}_{\text{CR}} = 5.13$ ).
- The reduction factor for chemical clogging is based on ranges provided by Keorner in GRI Guide GC8 ( $\text{RF}_{\text{CC}} = 1.5$ ).
- The reduction factor for biological clogging is based on ranges provided by Keorner in GRI Guide GC8 ( $\text{RF}_{\text{BC}} = 1.3$ ).

The resulting actual specified transmissivity is calculated as shown below:

$$\text{Transmissivity}_{\text{act}} = 3.048 * 10^{-6} \text{ m}^2/\text{sec} * 2 * (1.0 * 5.13 * 1.5 * 1.3) = 6.1 * 10^{-5} \text{ m}^2/\text{sec}.$$





## Civil & Environmental Consultants, Inc.

SUBJECT **Baseliner Leachate Detection Zone Geocomposite Transmissivity**

PROJECT NO. **302-918**

PROJECT **Phase 7 CCB Landfill Expansion**

PAGE **4** OF **4**

**Harrison Power Station**

MADE BY **AAW**

DATE **12/16/2020**

CHECKED BY

**TJK**

DATE

**3/12/2021**

### Geocomposite Permeability

The equivalent permeability of geocomposite is calculated as follows:

$$k_{act} = \theta_{act}/t$$

Where :

$K_{act}$  = Permeability of geocomposite

$\theta_{act}$  = Transmissivity of the geocomposite at time of installation

t = Thickness of the geocomposite

$$K_{act} = \frac{6.1 \times 10^{-5} \frac{m^2}{sec}}{(250 \text{ mil}) \left( \frac{1 \text{ in}}{1000 \text{ mil}} \right) \left( \frac{2.54 \text{ cm}}{\text{in}} \right)} \times \frac{10,000 \text{ cm}^2}{1 \text{ m}^2} = 0.960 \frac{\text{cm}}{\text{sec}}$$



### Testing Parameters

To accurately model field conditions, the selected geocomposite shall be tested at specified normal load as described below and in Table 6-1 of the CQA/QC Plan.

Testing shall be performed using deaired water, project geosynthetic clay liner for substrate, and project subbase soil compacted to 95% D698 maximum dry density at 3% to 5% wet of optimum moisture content for superstratum. Testing shall be performed at a hydraulic gradient of 0.33 ft/ft with the site specific boundary conditions of the baseliner system. For the West Liner area, a normal stress of 8,500 lb/ft<sup>2</sup> shall be applied with a seating period of 100 hours. If GDN is proposed in the East Liner area, a normal stress of 32,000 lb/ft<sup>2</sup> shall be applied with a seating period of 100 hours.

## CONCLUSIONS

### Geocomposite Requirements

The results of the geocomposite transmissivity calculation indicate that a transmissivity of **6.1 x 10<sup>-5</sup> m<sup>2</sup>/sec** is required. This value is specified for the Phase 7 Expansion areas.

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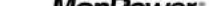
## **DRAWING**

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PROPOSED		
PREVIOUS		

VICINITY MAP

www.ccbcc.com				PHASE 7 CCB LANDFILL EXPANSION TITLE SHEET AND VICINITY MAP			
REFERENCE DRAWINGS				ENGINEERING	DATE		
DWG. NO.	TITLE		DR	JML	03/12/2002		
			CWD	MRP	03/12/2002		
			APP	DWT*	03/12/2002		
			SCALE				
				FACILITY HARRISON		UNIT	COMMON
						DWG. NO.	C89509681
						REV.	



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GENERAL:

1. THE SELLER IS RESPONSIBLE FOR FURNISHING AND INSTALLING EROSION AND SEDIMENTATION (E&S) CONTROLS FOR CONSTRUCTION. BEST MANAGEMENT PRACTICES (BMPs) SHALL BE INSTALLED IN ACCORDANCE WITH THE DETAILS AND MANUFACTURERS RECOMMENDATIONS.

2. THROUGHOUT CONSTRUCTION THE SELLER IS RESPONSIBLE FOR LOCATING AND PROTECTING PROPERTY CORNERS, UNDERGROUND UTILITIES, AND ABOVE GROUND UTILITIES. THE PROVIDED LOCATIONS OF UNDERGROUND UTILITIES ARE APPROXIMATE. THE SELLER IS RESPONSIBLE FOR CONTACTING UTILITY LOCATION SERVICES (MISS UTILITY OR WEST VIRGINIA 811) AND DETERMINING EXACT LOCATION OF UNDERGROUND UTILITIES. OTHER UNDERGROUND UTILITIES, NOT SHOWN ON PLANS, MAY BE PRESENT.

3. THE SELLER SHALL CLEAR AND GRUB THE WORK AREA TO PROVIDE SUFFICIENT CLEARANCE FOR COMPLETING WORK. CLEARING AND GRUBBING IS THE REMOVAL OF TREES, BRUSH, STUMPS AND ROOTS GREATER THAN ONE-HALF INCH IN DIAMETER. CLEARING AND GRUBBING SHALL BE PERFORMED PRIOR TO EXCAVATION OR FILL PLACEMENT. STUMPS, ROOTS, LOGS, STICKS AND OTHER PERISHABLE MATERIALS SHALL BE REMOVED TO A DEPTH OF AT LEAST 6 INCHES BELOW GROUND SURFACE. LARGE STUMPS MAY BE REMOVED DURING GRADING OPERATIONS, SUBJECT TO THE APPROVAL OF THE BUYERS AGENT. PREFERRED METHODS OF DISPOSAL IS ON-SITE PROCESSING WITH A TUB GRINDER OR BY PROVIDING MATERIAL FOR PULP WOOD HARVESTING.

4. BURNING OF CLEARED MATERIAL IS NOT PERMITTED.

5. AREAS WHERE SPRINGS, SOFT, OR POTENTIALLY UNSUITABLE SUBGRADE IS DETECTED SHALL BE BROUGHT TO THE BUYER'S REPRESENTATIVE'S ATTENTION IMMEDIATELY. THE BUYER'S REPRESENTATIVE IS THE SOLE JUDGE OF SUITABILITY OF SUBGRADE MATERIAL. THE SELLER SHALL CONTROL GROUNDWATER AND SEEPAGE FOR EXCAVATION OPERATIONS, SUBBASE AND SUBGRADE PREPARATION, AND LINER PLACEMENT.

6. THE SELLER SHALL MAINTAIN ON-SITE ROADWAYS USED FOR HAULING. MAINTENANCE INCLUDES WATERING, GRADING, LEVELING, REPLACEMENT, AND COMPACTION OF ROAD BASE REQUIRED TO REPAIR DAMAGE OF ROADWAYS.

7. THE MAP GRID SHOWN IS BASED ON THE WEST VIRGINIA COORDINATE SYSTEM, NORTH ZONE, 1983 NORTH AMERICAN DATUM.

EARTHWORK:

8. THE SELLER SHALL PROVIDE AND MAINTAIN DUST CONTROL DURING THE CONSTRUCTION. DUST CONTROL SHALL BE BY MEANS OF WETTING VIA WATER TRUCK.

9. PRIOR TO CONSTRUCTION, THE BUYER'S REPRESENTATIVE WILL SAMPLE AND TEST SUBBASE SOIL TO ESTABLISH THE MOISTURE/DENSITY RELATIONSHIPS NECESSARY TO ATTAIN THE REQUIRED IN-PLACE (COMPACTED) PERMEABILITIES. DURING CONSTRUCTION, TO EVALUATE COMPLIANCE WITH THE REQUIREMENTS, THE BUYER'S REPRESENTATIVE WILL SAMPLE SUBBASE SOIL AS IT IS PLACED IN ACCORDANCE WITH THE CONSTRUCTION QUALITY ASSURANCE AND QUALITY CONTROL PLAN.

10. THE SELLER SHALL STRIP TOPSOIL FROM EXCAVATION AND FILL AREAS TO FULL DEPTH, AND SHALL STOCKPILE STRIPPED TOPSOIL AS DIRECTED BY BUYER'S AGENT. ROCKS LARGER THAN ONE-HALF INCH IN DIAMETER SHALL BE REMOVED. TOPSOIL SHALL BE SEGREGATED FROM OTHER STOCKPILED SOILS AS DIRECTED BY THE BUYER'S AGENT. TOPSOIL THICKNESS MAY VARY. THE SELLER IS RESPONSIBLE FOR DETERMINING THE AMOUNT TO BE STRIPPED. REMOVE STONES, BRUSH, RUBBISH AND UNSUITABLE MATERIALS FROM TOPSOIL BEFORE STOCKPILING.

11. THE SELLER SHALL COMPLETE EXCAVATION AND FILLS TO THE LINES AND GRADES SHOWN ON THE DRAWINGS. FILL SLOPES SHALL BE OVER BUILT AND TRIMMED SO THE SLOPED SURFACE CONSISTS OF PROPERLY COMPACTED SOIL. EXCAVATED MATERIALS MAY INCLUDE SOIL, ROCK, ASH, ASH-SOIL MIXTURES, COAL, COAL CONTAMINATED SOILS, CARBOMACEOUS SHALE, SURFACE MINE BACKFILL, DEEP MINE BACKFILL, EXCESS UNCONTAMINATED SOIL, EXCESS ROCK AND EXCAVATED COAL MAY BE USED BY THE BUYER AND SHALL BE STOCKPILED AS DIRECTED BY BUYER'S AGENT. THE BUYER'S REPRESENTATIVE SHALL DETERMINE THE CLASSIFICATION OF THE EXCAVATION AREAS EXCAVATED BELOW DESIGN SUBGRADE ELEVATIONS BY THE SELLER, UNLESS REQUESTED BY THE BUYER'S REPRESENTATIVE, SHALL BE BROUGHT BACK TO DESIGN ELEVATIONS AT NO COST TO THE BUYER.

12. THE SELLER SHALL SMOOTH ROLL EXCAVATION AND FILL SURFACES AND BRING THE SURFACE TO WITHIN 0.2 FEET OF THE SPECIFIED GRADE. UNDER CONCRETE STRUCTURES, CHANNELS AND HAIL ROADS, THE SURFACE SHALL BE WITHIN 0.1 FEET OF THE SPECIFIED GRADE. AVOID CREATING LOW SPOTS WHICH COULD POND WATER. AREAS TO RECEIVE SEEDING SHALL BE TRACKED IN UP AND DOWN SLOPES WITH EQUIPMENT WITH CLEATED TRACKS, SEE TRACKING SLOPES DETAIL.

13. THE SELLER SHALL GRADE RESTORED BORROW AREAS, SOIL DISPOSAL PILES AND STOCKPILES NO STEEPER THAN 2H:1V (OR AS SHOWN ON THE DRAWINGS). GRADING SHALL AVOID IMPOUNDING WATER. STOCKPILES SHALL BE BENCHED EVERY 20 FEET IN ELEVATION. BENCHES SHALL BE A MINIMUM 20 FEET WIDE AND SHALL SLOPE TO PILE AT A MINIMUM 1 PERCENT SLOPE AND MAXIMUM 3 PERCENT SLOPE. STOCKPILES DISTURBED DURING CONSTRUCTION SHALL BE REGRADED UPON COMPLETING EARTHMOVING ACTIVITIES.

14. GRANULAR FILL SHALL BE PLACED IN UNIFORM HORIZONTAL LIFTS HAVING A MAXIMUM THICKNESS OF 12 INCHES. COMPACTION OF GRANULAR FILL SHALL ACHIEVED BY TRACKING THE MATERIAL IN PLACE TO VISUALLY OBSERVED NON-MOVEMENT.

15. FILL (STRUCTURAL FILL, GENERAL FILL, AND SUBBASE) SHALL COME FROM SITE GRADING OR DESIGNATED BORROW AREAS. PROCESSING (REMOVAL/CRUSHING OF ROCKS, SCREENING, OR MOISTURE CONTENT MODIFICATION) OF MATERIAL SHALL BE PERFORMED AT THE BORROW AREA. TOPSOIL AND SOIL UNFIT FOR USE SHALL BE REMOVED AND STOCKPILED.

16. FILL SHALL BE PLACED IN UNIFORM HORIZONTAL LIFTS. MATERIAL SHALL BE SCARIFIED BETWEEN LIFTS. DENSITY COMPACTION TESTING IS REQUIRED FOR EVERY LIFT REGARDLESS OF THICKNESS AT THE MINIMUM FREQUENCIES LISTED IN THE CONSTRUCTION QUALITY ASSURANCE AND QUALITY CONTROL PLAN. CORRECTIONS FOR UNIT WEIGHT AND WATER CONTENT OF SOILS CONTAINING OVERSIZED PARTICLES SHALL BE IN ACCORDANCE WITH ASTM D4718. COMPACTED SURFACES SHALL MEET SPECIFIED DENSITY AND MOISTURE CRITERIA IMMEDIATELY PRIOR TO PLACEMENT OF THE NEXT LIFT.

17. BEFORE PLACEMENT OF THE LIFT, SUBGRADE AND AREAS TO RECEIVE FILL SHALL BE PROOF ROLLED. THE BUYER'S REPRESENTATIVE SHALL BE PRESENT FOR COMPACTION. LIFT SHALL BE COMPACTED TO 95% OF THE ASTM D698 MAXIMUM DRY DENSITY.

18. FILL WITHIN THREE FEET OF STRUCTURES, PIPES, AND IN AREAS WHERE LARGER EQUIPMENT CAN NOT BE OPERATED SHALL BE COMPACTED WITH HAND DIRECTED POWER EQUIPMENT. WHERE HAND-DIRECTED EQUIPMENT IS USED, THE MAXIMUM ALLOWABLE LIFT THICKNESS SHALL BE FOUR INCHES AND MAXIMUM ALLOWABLE ROCK FRAGMENT SIZE SHALL BE THREE INCHES).

19. THE COMPACTION TESTER SHALL IMMEDIATELY BACKFILL HOLES FROM TESTING IN SUBBASE, SUBGRADE OR CLAY LINER. HOLES SHALL BE BACKFILLED WITH POWDERED BENTONITE AND TAMPPED WITH A ROD IN 12 INCH MAXIMUM LIFTS TO WITHIN 1 INCH OF THE SURFACE. WATER SHALL THEN BE ADDED TO THE UPPER 1 INCH OF THE HOLE.

20. IN AREAS WHERE COMPACTION CRITERIA CANNOT BE MET DUE TO MOISTURE FROM SPRINGS, THE SUBGRADE DRAINAGE/LEACHATE DETECTION SYSTEM SHALL BE EXTENDED TO INTERCEPT THESE SPRINGS AS DIRECTED BY AND IN THE PRESENCE OF THE BUYER'S REPRESENTATIVE.

21. IN AREAS WHERE "PUMPING" OF THE SOIL IS OBSERVED BY BUYER'S REPRESENTATIVE, UNSUITABLE MATERIAL MAY BE OVER EXCAVATED AND REPLACED AS DIRECTED BY AND IN THE PRESENCE OF THE BUYER'S REPRESENTATIVE.

22. SOIL FOR GENERAL AND SUBGRADE FILL CONSTRUCTION SHALL MEET THE FOLLOWING REQUIREMENTS:

A. BE CLASSIFIED AS SM, SC, ML, MH, CH, CL, OR CL-ML USING THE UNIFIED SOIL CLASSIFICATION SYSTEM.

B. HAVE A MAXIMUM PARTICLE SIZE OF THREE (3)-INCHES (STRUCTURAL FILL) OR NINE (9)-INCHES (GENERAL FILL).

C. BE PLACED IN SIX (6)-INCH (SUBGRADE FILL) OR TWELVE (12)-INCH (GENERAL FILL) MAXIMUM COMPACTED LIFTS.

D. BE PLACED AT MINUS 4% TO PLUS 4% OF THE ASTM D698 OPTIMUM MOISTURE CONTENT.

E. BE COMPACTED TO 95% OF THE ASTM D698 MAXIMUM DRY DENSITY.

23. SOIL FOR LINER SYSTEM SUBBASE CONSTRUCTION SHALL MEET THE FOLLOWING REQUIREMENTS:

A. HAVE A MAXIMUM PARTICLE SIZE OF TWO (2) INCHES.

B. BE PLACED IN SIX (6)-INCH MAXIMUM COMPACTED LIFTS.

C. BE PLACED AT PLUS 3 % TO PLUS 5% OF THE ASTM D698 OPTIMUM MOISTURE CONTENT.

D. BE COMPACTED TO 95% OF THE ASTM D698 MAXIMUM DRY DENSITY.

E. HAVE AN IN-PLACE (COMPACTED) PERMEABILITY NO MORE THAN 1 x 10<sup>-10</sup> CM/SEC.

24. \*NON-RESISTANT ROCK\* FILLS MAY BE PLACED AS APPROVED BY THE BUYER'S REPRESENTATIVE.

A. THE TERM "NON-RESISTANT ROCK" IS DEFINED AS MATERIAL WHICH CAN BE BROKEN DOWN AND DISINTEGRATED DURING NORMAL COMPACTION WITH MECHANICAL EQUIPMENT AND INCLUDES SOFT WEATHERED ROCKS SUCH AS CLAYTONES AND SOME SHALES.

B. NON-RESISTANT ROCK FILL SHALL BE CRUSHED AND BROKEN BY THE ACTION OF A 20 TON SHEEPSFOOT ROLLER TOWED BY A D-9 BULLDOZER (OR AN APPROVED EQUAL), IF, IN THE OPINION OF THE BUYER'S AGENT, THE ABOVE SPECIFIED EQUIPMENT IS NOT CAPABLE OF SATISFACTORILY CRUSHING AND DISINTEGRATING ROCK. A CATERPILLAR 825 C COMPACTOR OR A 30-TON DISC WITH A BLADE DIAMETER OF AT LEAST 18 INCHES SHALL BE USED. AFTER THE NON-RESISTANT ROCK HAS BEEN SATISFACTORILY DISINTEGRATED TO A COHESIVE FILL MATERIAL, IT SHALL BE COMPACTED TO NON-MOVEMENT BY VISUAL INSPECTION.

C. THE TERM "RESISTANT ROCK", IS DEFINED AS MATERIAL OF SUCH HARDNESS AS CANNOT PRACTICALLY BE BROKEN DOWN AND DISINTEGRATED DURING NORMAL COMPACTION AND WHICH IS RESISTANT TO WEATHERING AND DECOMPOSITION. THIS INCLUDES MEDIUM HARD AND HARD SANDY SHALE, SANDSTONE, SILTSTONE AND LIMESTONE. RESISTANT ROCK FILL SHALL BE PLACED ONLY WHERE APPROVED BY THE BUYER'S REPRESENTATIVE.

D. THE RESISTANT ROCK FILL SHALL BE WELL GRADED AND THE LIFT THICKNESS LIMITED TO 3 FEET. AS RESISTANT ROCK IS PLACED, IT SHALL BE SPREAD AND WORKED INTO A STABLE ARRANGEMENT SO THAT THE INDIVIDUAL BOULDERS AND FRAGMENTS DO NOT REORIENT THEMSELVES UNDER THE WEIGHT OF OVERLYING MATERIAL. REWORKING OF EACH LIFT SHALL BE CONDUCTED TO OBTAIN THE GREATEST AMOUNT OF DENSIIFICATION PRACTICAL.

E. DURING FILL PLACEMENT OR REWORKING PROCESS THE VOID SPACES BETWEEN LARGE BOULDERS SHOULD BE FILLED WITH SMALLER SIZED ROCKS. THE DESIRED RESULTS IN A ROCK FILL IS TO PRODUCE A REASONABLY WELL-GRADED GRANULAR FILL WITH NO LARGE VOIDS OR OBJECTIONABLE POCKETS OF SMALL ROCKS OR CLUSTERS OF LARGE ROCKS.

F. RESISANT ROCK FILLS SHALL NOT BE PLACED FOR SUPPORTING OF STRUCTURES IF: INDIVIDUAL ROCK OR ROCKS INTERFERE WITH PROPER AND SMOOTH COMPACTION, THE ROCK SHOULD BE REMOVED FROM THE LIFT BY THE SELLER AND DISPOSED OF AS APPROVED BY THE BUYER'S AGENT.

G. EACH LIFT OF RESISTANT ROCK FILL SHALL HAVE A MAXIMUM PARTICLE SIZE OF 24 INCHES AND SHALL BE SUBJECTED TO A MINIMUM OF 4 PASSES OF A VIBRATORY ROLLER HAVING A MINIMUM IMPACT FORCE OF 30 TONS OR 8 PASSES OF A VIBRATORY ROLLER HAVING A MINIMUM IMPACT FORCE OF 15 TONS. THE FREQUENCY OF VIBRATION DURING OPERATION SHOULD BE BETWEEN 1100 AND 1500 VIBRATIONS PER MINUTE. THE ROLLER SHOULD BE OPERATED AT A SPEED NOT TO EXCEED 3 MILES PER HOUR. WHEN USED, ROLLERS ARE USED. THEY SHOULD BE TOWED BY A CRAWLER TYPE TRACTOR OR BULLDOZER IN A FORWARD MOTION ONLY. SUCCESSIVE PASSES OF ROLLERS SHOULD OVERLAP.

25. AT THE END OF EACH DAY, OR WHEN WORK IS STOPPED COMPACTED EARTH FILL AND NON-RESISTANT ROCK FILL SURFACES SHALL BE SMOOTH-ROLLED AND EXPOSED ENDS OF AGGREGATE SHALL BE COVERED BY FOLDING GEOTEXTILE FROM THE LOWER LIFT OVER THE EDGE. THE INTENT IS TO MINIMIZE EROSION, PONDING, AND INFILTRATION OF WATER.

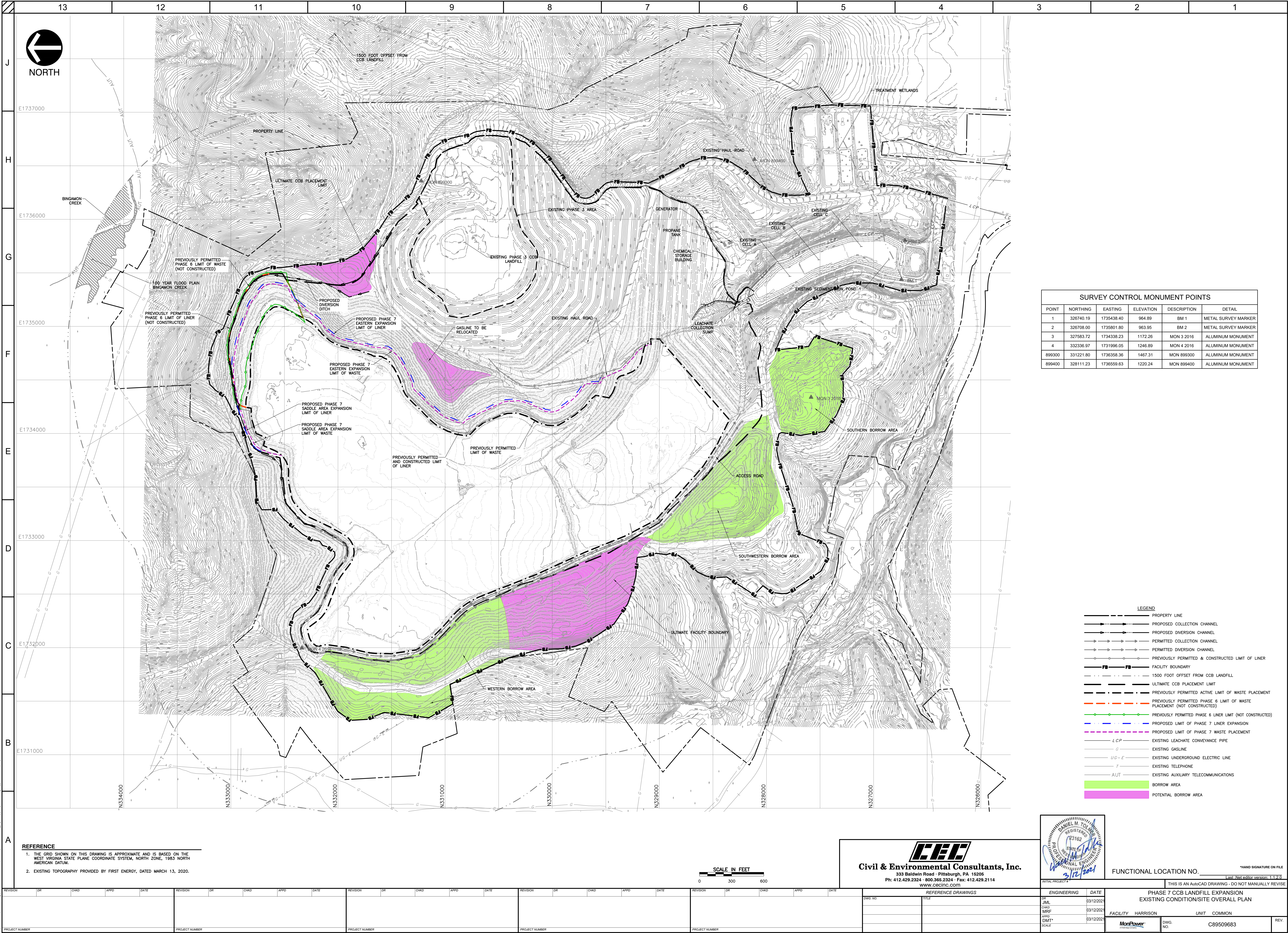
26. BLASTING MAY BE ALLOWED, SUBJECT TO PRIOR APPROVAL BY THE BUYER'S AGENT. BLASTING SHALL CONFORM TO GOVERNMENTAL AGENCY REGULATIONS AND STANDARDS. THE SELLER SHALL SUBMIT A PROPOSED BLASTING PROGRAM TO THE BUYER FOR REVIEW A MINIMUM OF 2 WEEKS PRIOR TO THE START OF BLASTING. REVIEW DOES NOT REMOVE ANY LIABILITY FROM THE SELLER. THE SELLER SHALL COORDINATE BLASTING WITH THE BUYER'S AGENT. IF IN THE OPINION OF THE BUYER'S AGENT OR BUYER'S REPRESENTATIVE, APPROPRIATE CHARGES APPEAR EXCESSIVE, THE SELLER MAY BE REQUIRED TO PERFORM BLAST MONITORING AT LOCATIONS DETERMINED BY THE BUYER'S AGENT AT NO ADDITIONAL COST TO THE BUYER. DAMAGE TO STRUCTURES CAUSED BY BLASTING OPERATION SHALL BE REPAIRED BY THE SELLER AT NO ADDITIONAL COST TO THE BUYER OR BUYER'S REPRESENTATIVE. THE SELLER SHALL NOT BE PAID FOR ANY ROCK BREAKAGE BEYOND THE NEAT LINE OF THE EXCAVATION AND SHALL REMOVE ANY LOOSE MATERIAL AND BACKFILL ANY OVERBREAK AREAS WITH SUBGRADE MATERIAL MEETING THE SPECIFICATIONS. THE COST FOR THE BLASTING, IS TO BE INCLUDED WITH THE COST FOR EXCAVATION.

9

PIPEING:

27. THE LEACHATE DETECTION AND LEACHATE COLLECTION PIPE SYSTEMS SHALL BE HIGH DENSITY POLYETHYLENE (HDPE) PERFORATED PIPE HOLE SIZES AND LOCATIONS ARE SHOWN ON THE DRAWINGS. PIPE SHALL BE JOINED BY BUTT FUSION, ELECTRIC FUSION COLLARS, OR BUYER APPROVED COUPLERS. FABRICATED FITTINGS SHALL BE REQUIRED FOR FITTINGS AND CHANGES IN DIRECTION OR GRADE BEYOND THE MANUFACTURER'S RECOMMENDED PRACTICE. THE SELLER SHALL FURNISH "AS-BUILT" SURVEYED COORDIN





SURVEY CONTROL MONUMENT POINTS					
POINT	NORTHING	EASTING	ELEVATION	DESCRIPTION	DETAIL
1	326740.19	1735438.40	964.89	BM 1	METAL SURVEY MARKER
2	326708.00	1735801.80	963.95	BM 2	METAL SURVEY MARKER
3	327583.72	1734338.23	1172.26	MON 3 2016	ALUMINUM MONUMENT
4	332336.97	1731996.05	1246.89	MON 4 2016	ALUMINUM MONUMENT
899300	331221.80	1736358.36	1467.31	MON 899300	ALUMINUM MONUMENT
899400	328111.23	1736559.63	1220.24	MON 899400	ALUMINUM MONUMENT

- LEGEND
- PROPERTY LINE
  - PROPOSED COLLECTION CHANNEL
  - PROPOSED DIVERSION CHANNEL
  - PERMITTED COLLECTION CHANNEL
  - PERMITTED DIVERSION CHANNEL
  - PREVIOUSLY PERMITTED & CONSTRUCTED LIMIT OF LINER
  - FACILITY BOUNDARY
  - 1500 FOOT OFFSET FROM CCB LANDFILL
  - ULTIMATE CCB PLACEMENT LIMIT
  - PREVIOUSLY PERMITTED ACTIVE LIMIT OF WASTE PLACEMENT
  - PREVIOUSLY PERMITTED PHASE 6 LIMIT OF WASTE PLACEMENT (NOT CONSTRUCTED)
  - PROPOSED LIMIT OF PHASE 7 LINER EXPANSION
  - PROPOSED LIMIT OF PHASE 7 WASTE PLACEMENT
  - EXISTING LEACHATE CONVEYANCE PIPE
  - EXISTING GASLINE
  - EXISTING UNDERGROUND ELECTRIC LINE
  - EXISTING TELEPHONE
  - EXISTING AUXILIARY TELECOMMUNICATIONS
  - BORROW AREA
  - POTENTIAL BORROW AREA

REFERENCE

1. THE GRID SHOWN ON THIS DRAWING IS APPROXIMATE AND IS BASED ON THE WEST VIRGINIA STATE PLANE COORDINATE SYSTEM, NORTH ZONE, 1983 NORTH AMERICAN DATUM.

2. EXISTING TOPOGRAPHY PROVIDED BY FIRST ENERGY, DATED MARCH 13, 2020.

**Civil & Environmental Consultants, Inc.**  
333 Baldwin Road • Pittsburgh, PA 15205  
Ph: 412.429.2324 • 800.365.2324 • Fax: 412.429.2114  
www.ccecinc.com



FUNCTIONAL LOCATION NO. \_\_\_\_\_ \*HAND SIGNATURE ON FILE

REVISION					REVISION					REVISION					REVISION					REVISION				
DR	CHWD	APPD	DATE		DR	CHWD	APPD	DATE		DR	CHWD	APPD	DATE		DR	CHWD	APPD	DATE		DR	CHWD	APPD	DATE	
PROJECT NUMBER					PROJECT NUMBER					PROJECT NUMBER					PROJECT NUMBER					PROJECT NUMBER				

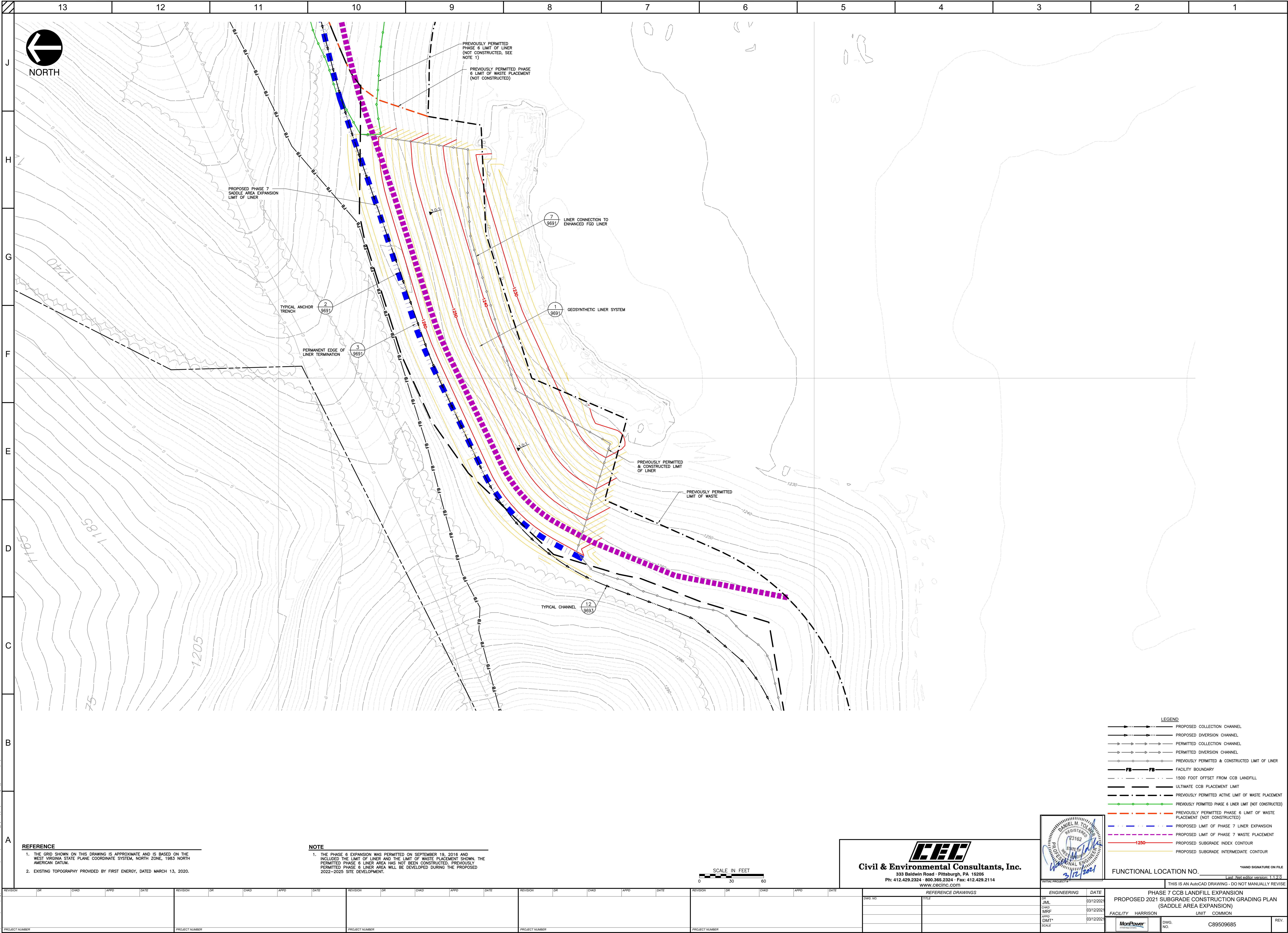
REFERENCE DRAWINGS		ENGINEERING		DATE		PHASE 7 CCB LANDFILL EXPANSION		EXISTING CONDITION/SITE OVERALL PLAN	
DWG. NO.	TITLE	DR	JML	03/12/2021		FACILITY	HARRISON	UNIT	COMMON
		CHWD	MRP	03/12/2021					
		APPD	DMT	03/12/2021					
		SCALE							

DWG. NO.	C89509683	REV.	
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**REFERENCE**

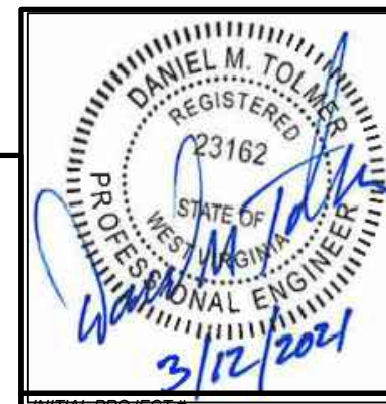
1. THE GRID SHOWN ON THIS DRAWING IS APPROXIMATE AND IS BASED ON THE WEST VIRGINIA STATE PLANE COORDINATE SYSTEM, NORTH ZONE, 1983 NORTH AMERICAN DATUM.

2. EXISTING TOPOGRAPHY PROVIDED BY FIRST ENERGY, DATED MARCH 13, 2020.

**NOTE**

1. THE PHASE 6 EXPANSION WAS PERMITTED ON SEPTEMBER 19, 2016 AND INCLUDED THE LIMIT OF LINER AND THE LIMIT OF WASTE PLACEMENT SHOWN. THE PERMITTED PHASE 6 LINER AREA HAS NOT BEEN CONSTRUCTED. PREVIOUSLY PERMITTED PHASE 6 LINER AREA WILL BE DEVELOPED DURING THE PROPOSED 2022-2025 SITE DEVELOPMENT.

- LEGEND**
- PROPOSED COLLECTION CHANNEL
  - PROPOSED DIVERSION CHANNEL
  - PERMITTED COLLECTION CHANNEL
  - PERMITTED DIVERSION CHANNEL
  - PREVIOUSLY PERMITTED & CONSTRUCTED LIMIT OF LINER
  - FACILITY BOUNDARY
  - 1500 FOOT OFFSET FROM CCB LANDFILL
  - ULTIMATE CCB PLACEMENT LIMIT
  - PREVIOUSLY PERMITTED ACTIVE LIMIT OF WASTE PLACEMENT
  - PREVIOUSLY PERMITTED PHASE 6 LINER LIMIT (NOT CONSTRUCTED)
  - PREVIOUSLY PERMITTED PHASE 6 LIMIT OF WASTE PLACEMENT (NOT CONSTRUCTED)
  - PROPOSED LIMIT OF PHASE 7 LINER EXPANSION
  - PROPOSED LIMIT OF PHASE 7 WASTE PLACEMENT
  - PROPOSED SUBGRADE INDEX CONTOUR
  - PROPOSED SUBGRADE INTERMEDIATE CONTOUR



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PROJECT NUMBER					PROJECT NUMBER					PROJECT NUMBER					PROJECT NUMBER					PROJECT NUMBER				

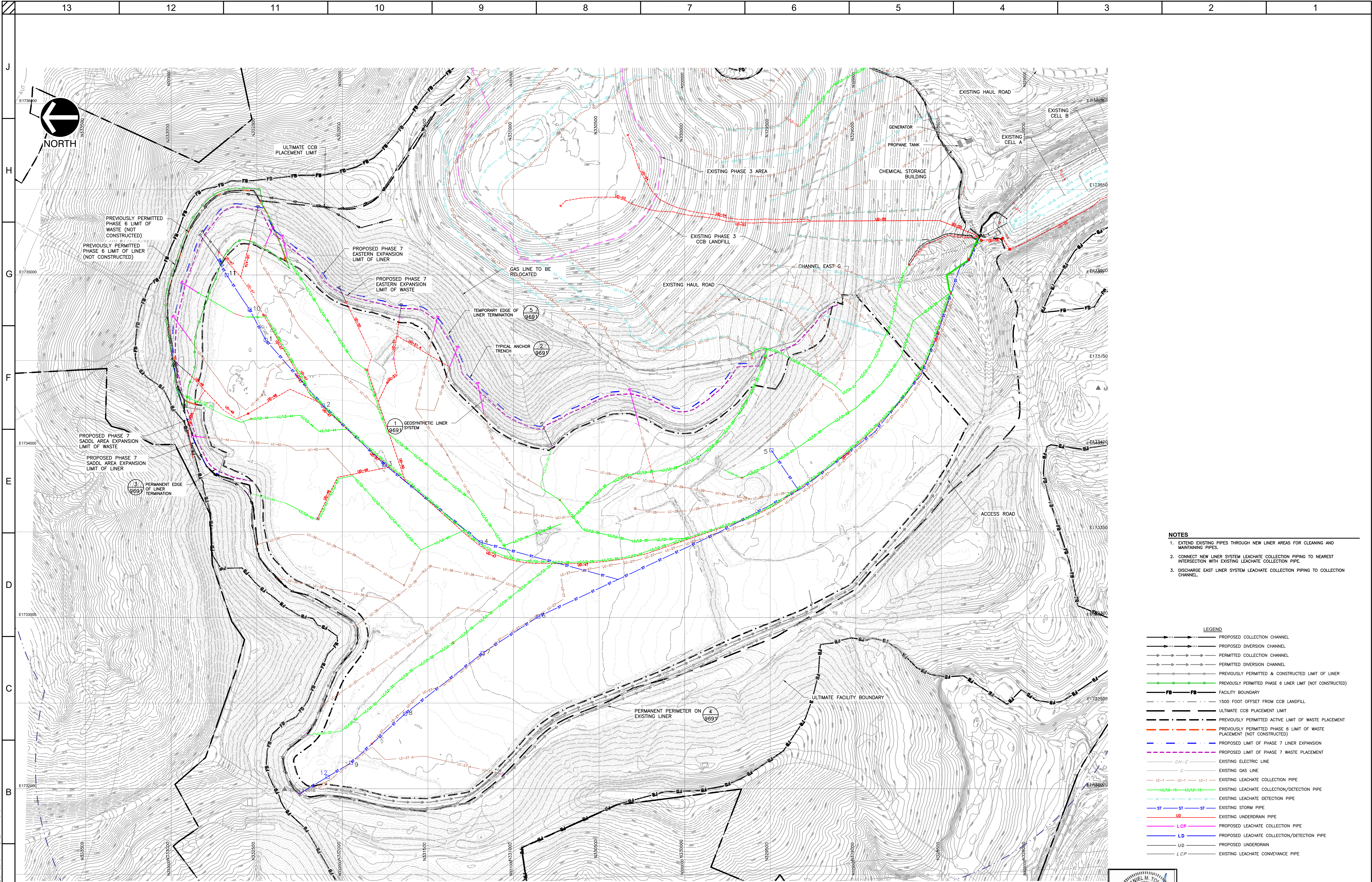
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DR	JML	03/12/2021							
CHWD	MRF	03/12/2021							
APPD	DMT	03/12/2021							
SCALE									

PHASE 7 CCB LANDFILL EXPANSION PROPOSED 2021 SUBGRADE CONSTRUCTION GRADING PLAN (SADDLE AREA EXPANSION)				DWG. NO.		REV.	
FACILITY HARRISON UNIT COMMON				C89509685			









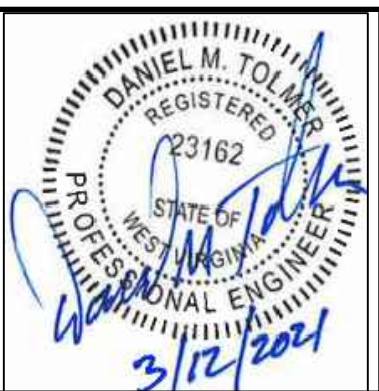
- NOTES**
1. EXTEND EXISTING PIPES THROUGH NEW LINER AREAS FOR CLEANING AND MAINTAINING PIPES.
  2. CONNECT NEW LINER SYSTEM LEACHATE COLLECTION PIPING TO NEAREST INTERSECTION WITH EXISTING LEACHATE COLLECTION PIPE.
  3. DISCHARGE EAST LINER SYSTEM LEACHATE COLLECTION PIPING TO COLLECTION CHANNEL.

- LEGEND**
- PROPOSED COLLECTION CHANNEL
  - PROPOSED DIVERSION CHANNEL
  - PERMITTED COLLECTION CHANNEL
  - PERMITTED DIVERSION CHANNEL
  - PREVIOUSLY PERMITTED & CONSTRUCTED LIMIT OF LINER
  - PREVIOUSLY PERMITTED PHASE 6 LINER LIMIT (NOT CONSTRUCTED)
  - FACILITY BOUNDARY
  - 1500 FOOT OFFSET FROM CCB LANDFILL
  - ULTIMATE CCB PLACEMENT LIMIT
  - PREVIOUSLY PERMITTED ACTIVE LIMIT OF WASTE PLACEMENT
  - PREVIOUSLY PERMITTED PHASE 6 LIMIT OF WASTE PLACEMENT (NOT CONSTRUCTED)
  - PROPOSED LIMIT OF PHASE 7 LINER EXPANSION
  - PROPOSED LIMIT OF PHASE 7 WASTE PLACEMENT
  - EXISTING ELECTRIC LINE
  - EXISTING GAS LINE
  - EXISTING LEACHATE COLLECTION PIPE
  - EXISTING LEACHATE COLLECTION/DETECTION PIPE
  - EXISTING LEACHATE DETECTION PIPE
  - EXISTING STORM PIPE
  - EXISTING UNDERDRAIN PIPE
  - PROPOSED LEACHATE COLLECTION PIPE
  - PROPOSED LEACHATE COLLECTION/DETECTION PIPE
  - PROPOSED UNDERDRAIN
  - EXISTING LEACHATE CONVEYANCE PIPE

- REFERENCE**
1. THE GRID SHOWN ON THIS DRAWING IS APPROXIMATE AND IS BASED ON THE WEST VIRGINIA STATE PLANE COORDINATE SYSTEM, NORTH ZONE, 1983 NORTH AMERICAN DATUM.
  2. EXISTING TOPOGRAPHY PROVIDED BY FIRST ENERGY, DATED MARCH 13, 2020.

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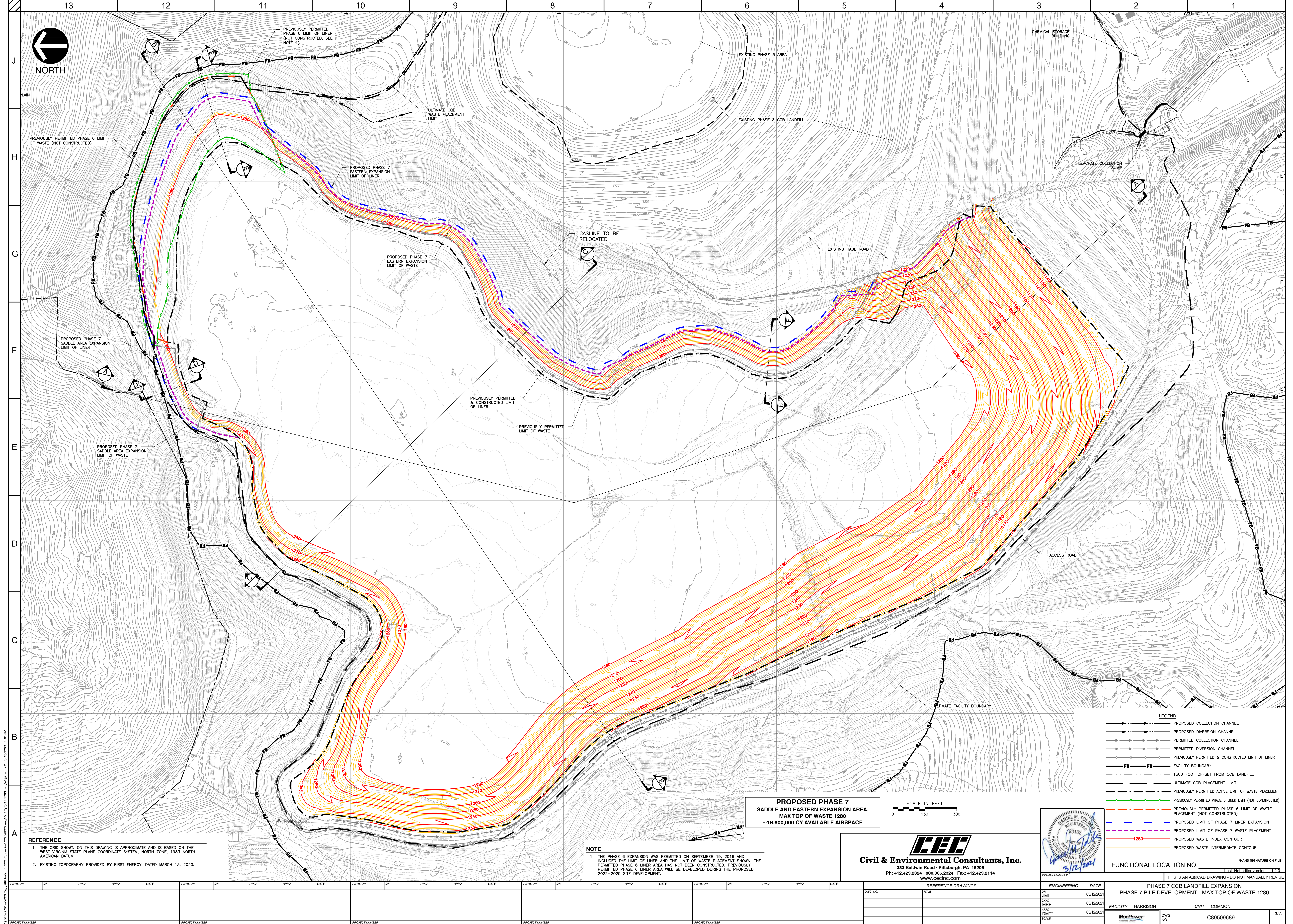
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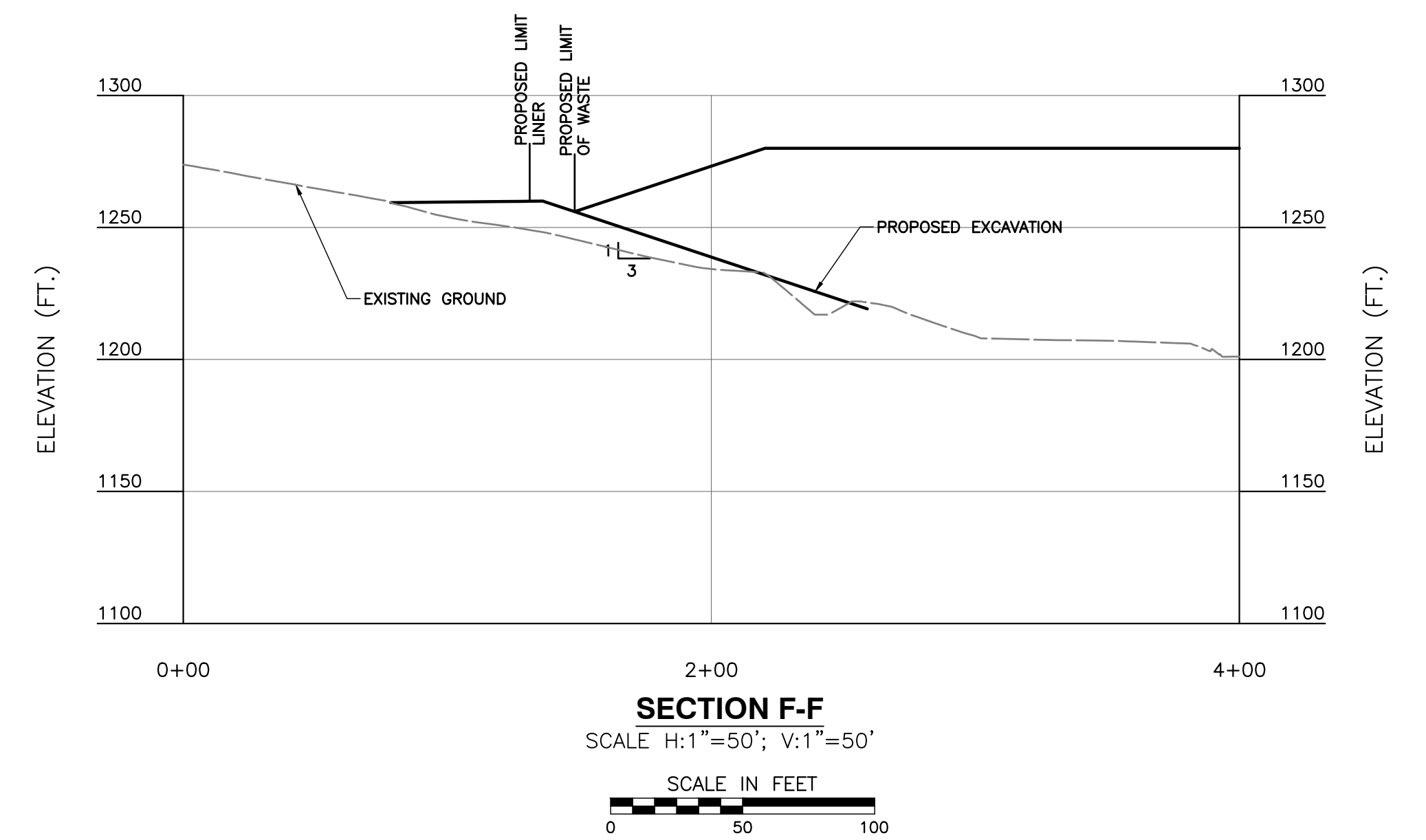
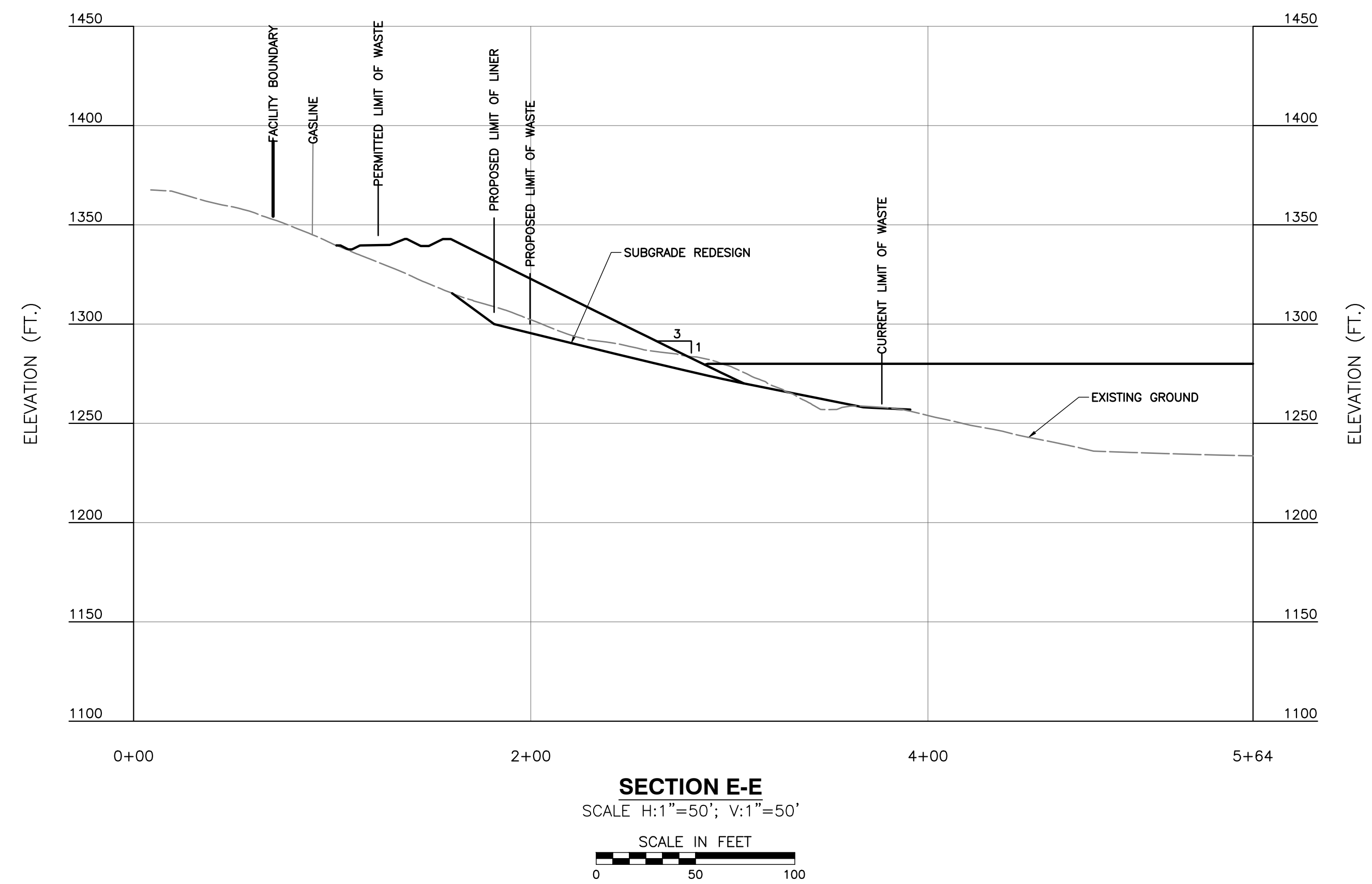
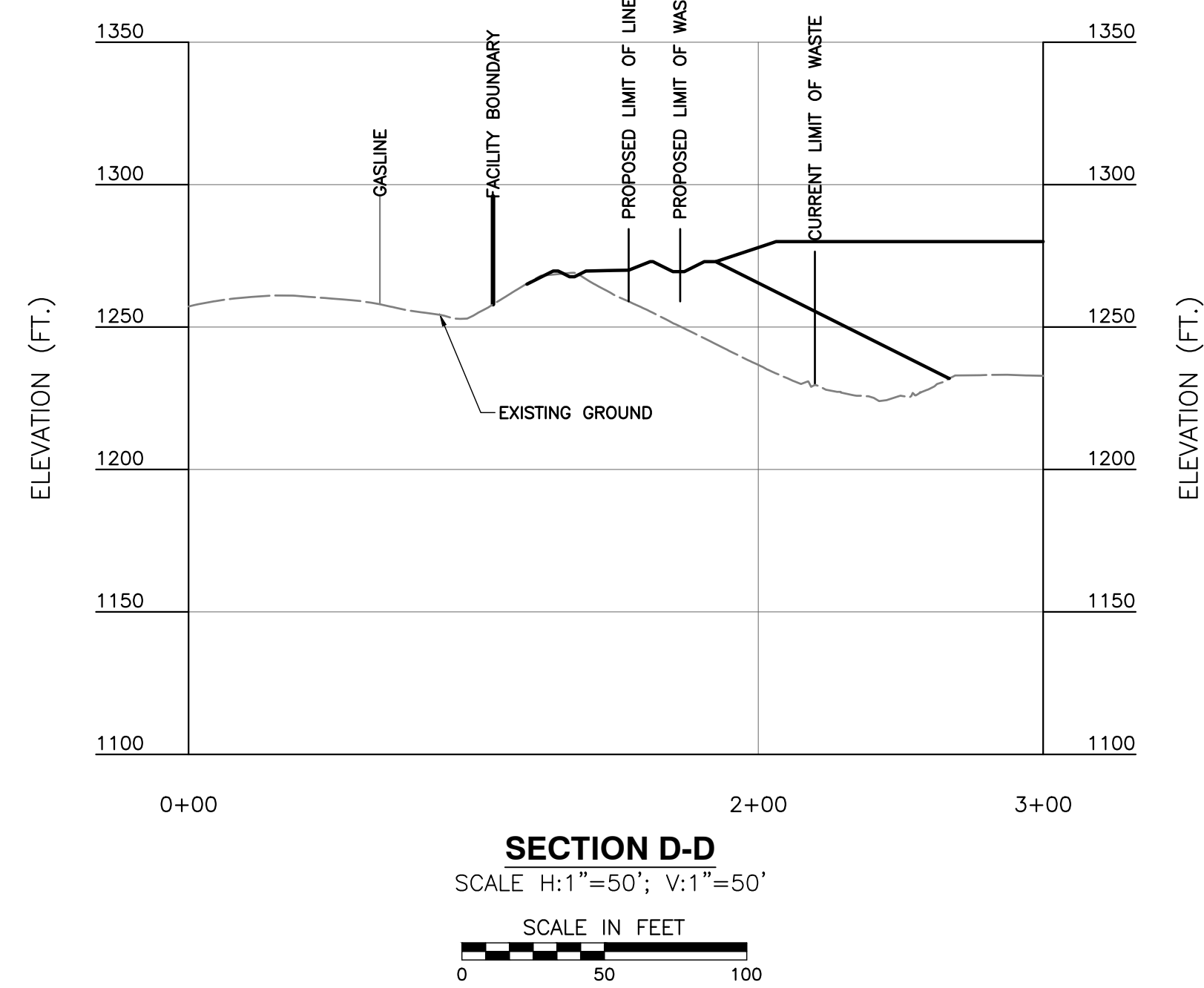
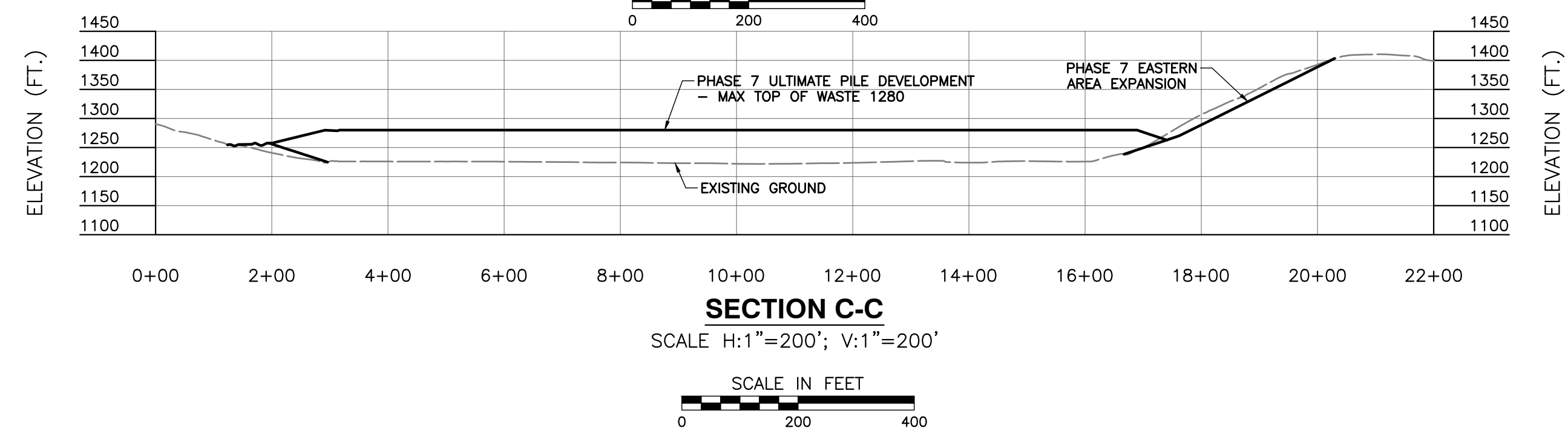
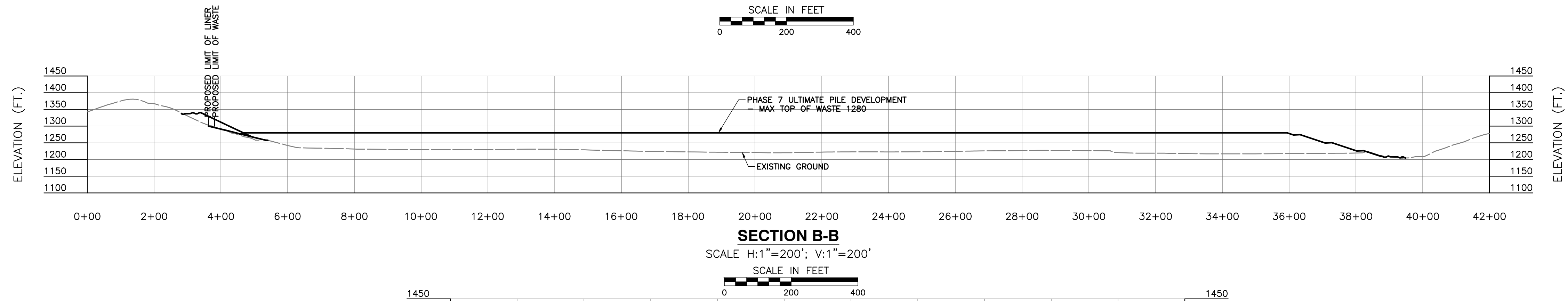
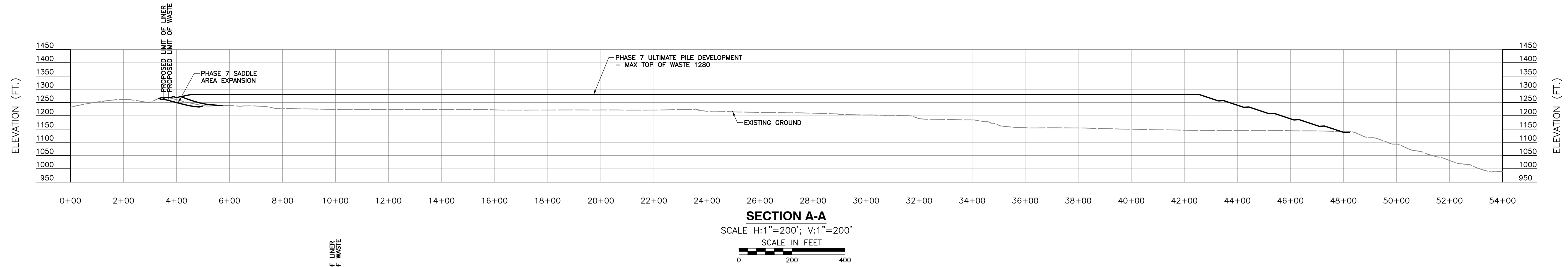












## REFERENCE

1. THE GRID SHOWN ON THIS DRAWING IS APPROXIMATE AND IS BASED ON THE WEST VIRGINIA STATE PLANE COORDINATE SYSTEM, NORTH ZONE, 1983 NORTH AMERICAN DATUM.
2. EXISTING TOPOGRAPHY PROVIDED BY FIRST ENERGY, DATED MARCH 13, 2020.

### LEGEND

----- APPROXIMATE EXISTING GROUND  
 \_\_\_\_\_ PROPOSED GROUND

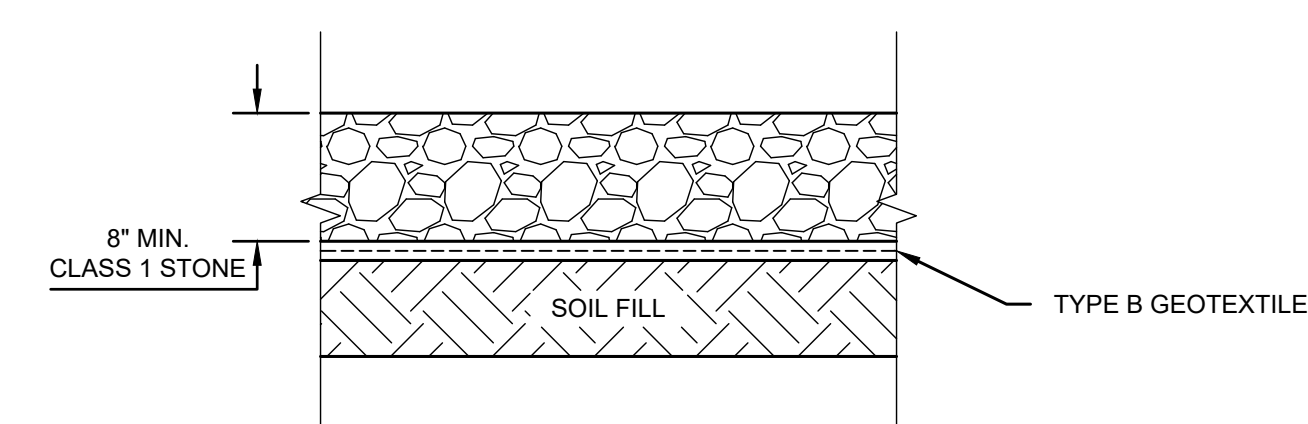
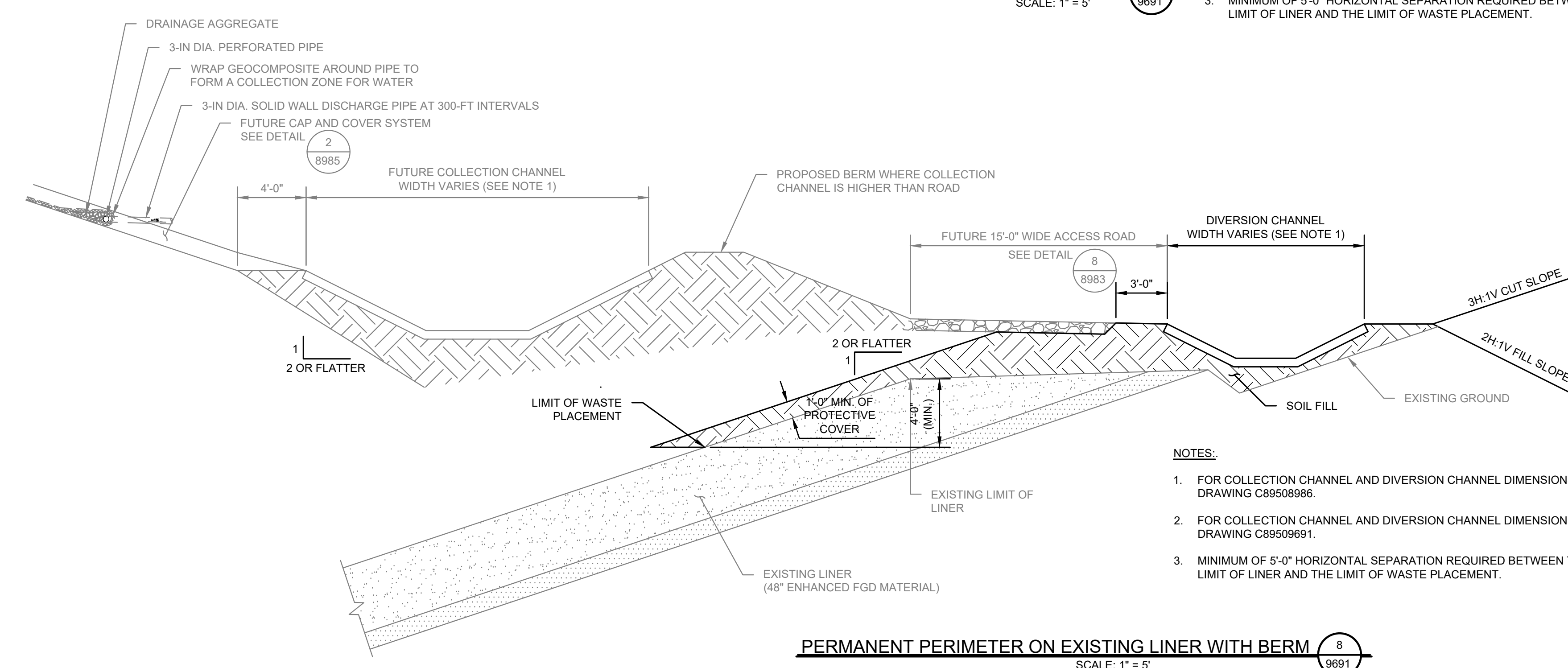
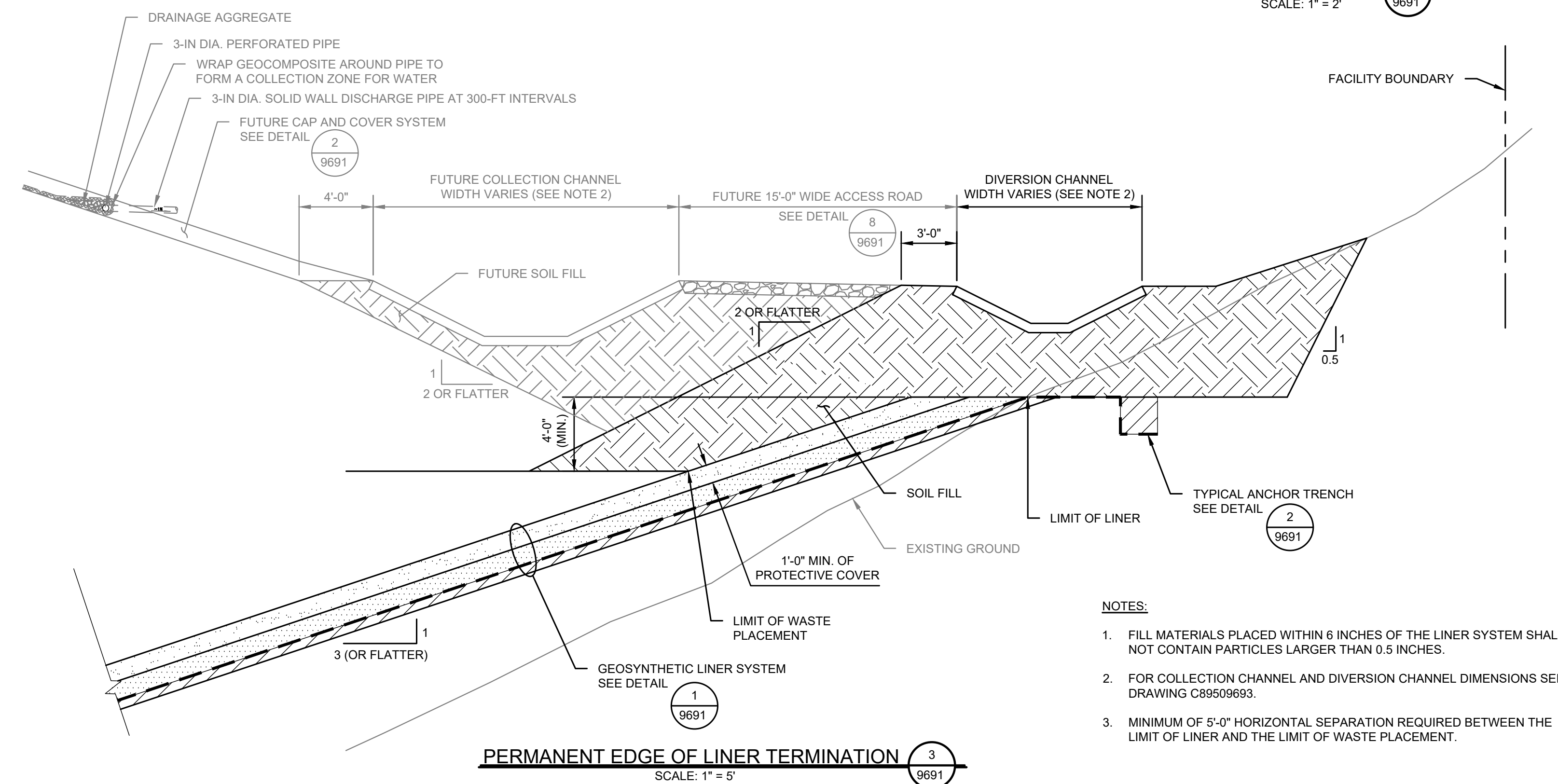
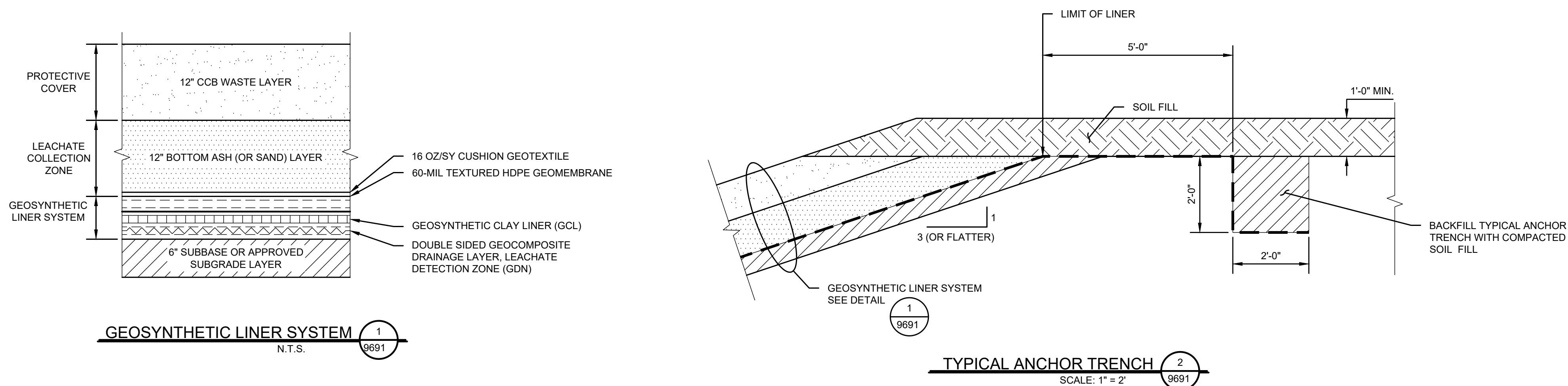
  
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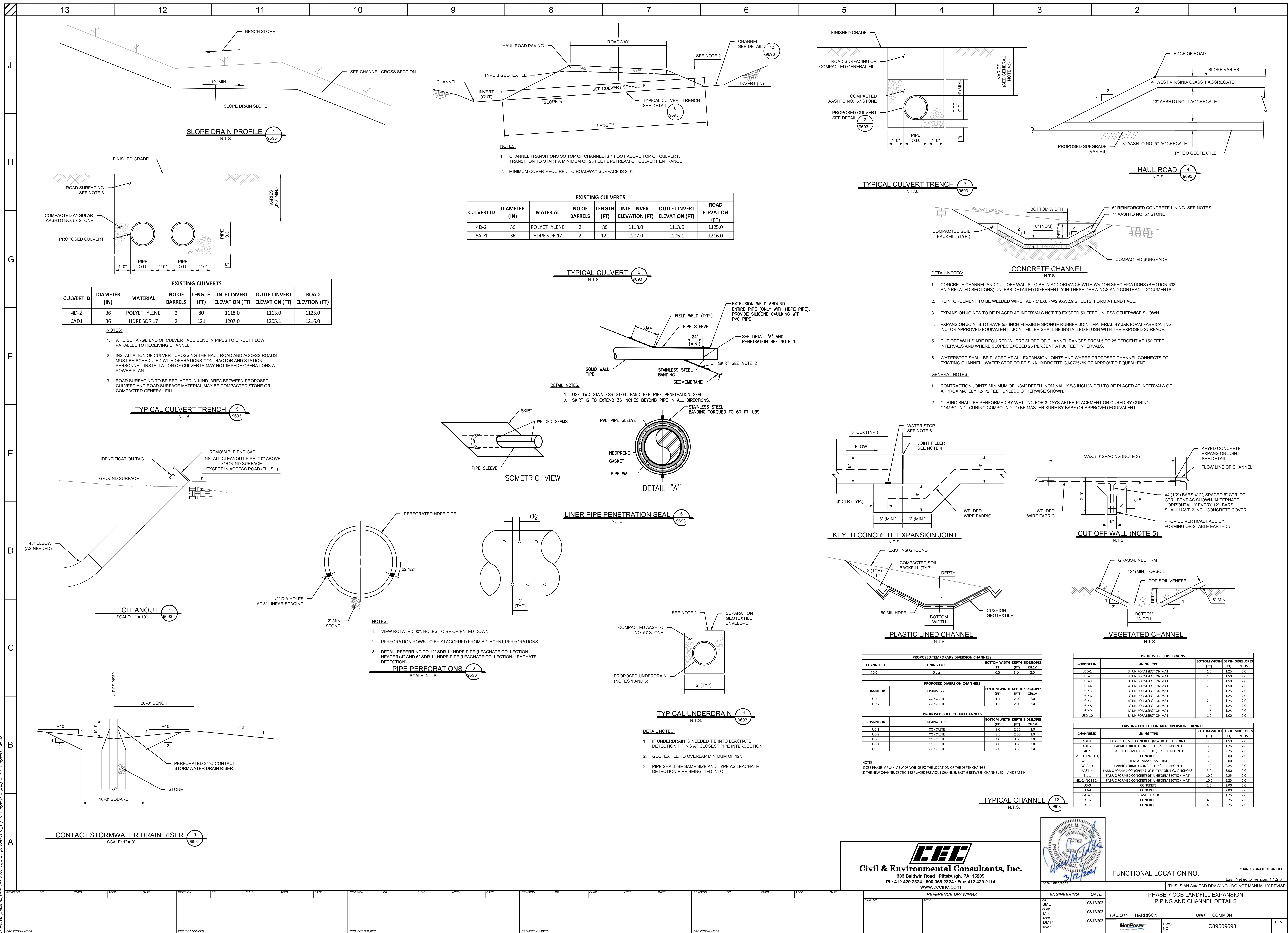
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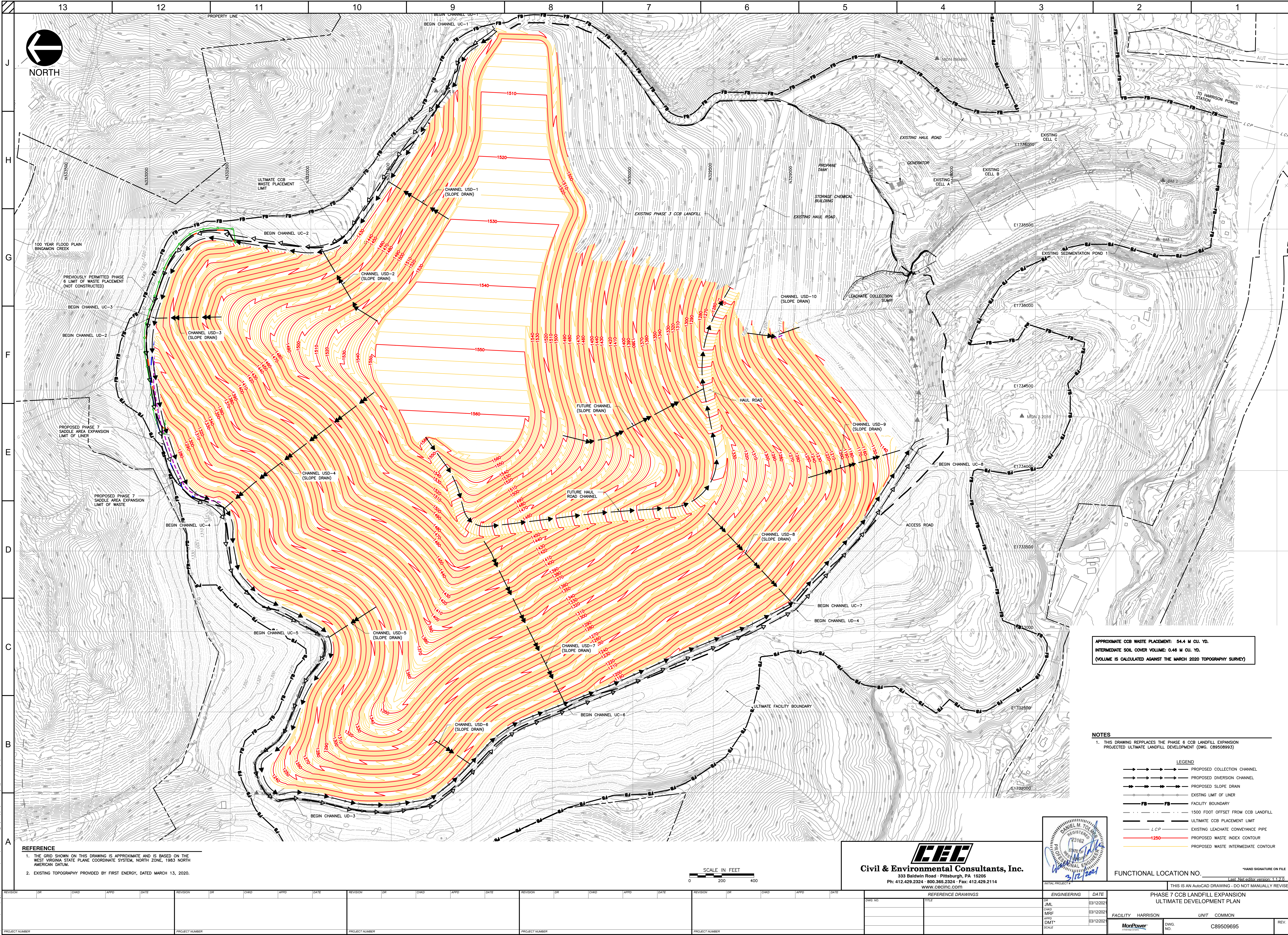












**REFERENCE**

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2. EXISTING TOPOGRAPHY PROVIDED BY FIRST ENERGY, DATED MARCH 13, 2020.

APPROXIMATE CCB WASTE PLACEMENT: 54.4 M CU. YD.  
INTERMEDIATE SOIL COVER VOLUME: 0.46 M CU. YD.  
(VOLUME IS CALCULATED AGAINST THE MARCH 2020 TOPOGRAPHY SURVEY)

**NOTES**

1. THIS DRAWING REPLACES THE PHASE 6 CCB LANDFILL EXPANSION PROJECTED ULTIMATE LANDFILL DEVELOPMENT (DWG. C89508993)

- LEGEND**
- PROPOSED COLLECTION CHANNEL
  - PROPOSED DIVERSION CHANNEL
  - PROPOSED SLOPE DRAIN
  - EXISTING LIMIT OF LINER
  - FACILITY BOUNDARY
  - 1500 FOOT OFFSET FROM CCB LANDFILL
  - ULTIMATE CCB PLACEMENT LIMIT
  - EXISTING LEACHATE CONVEYANCE PIPE
  - PROPOSED WASTE INDEX CONTOUR
  - PROPOSED WASTE INTERMEDIATE CONTOUR

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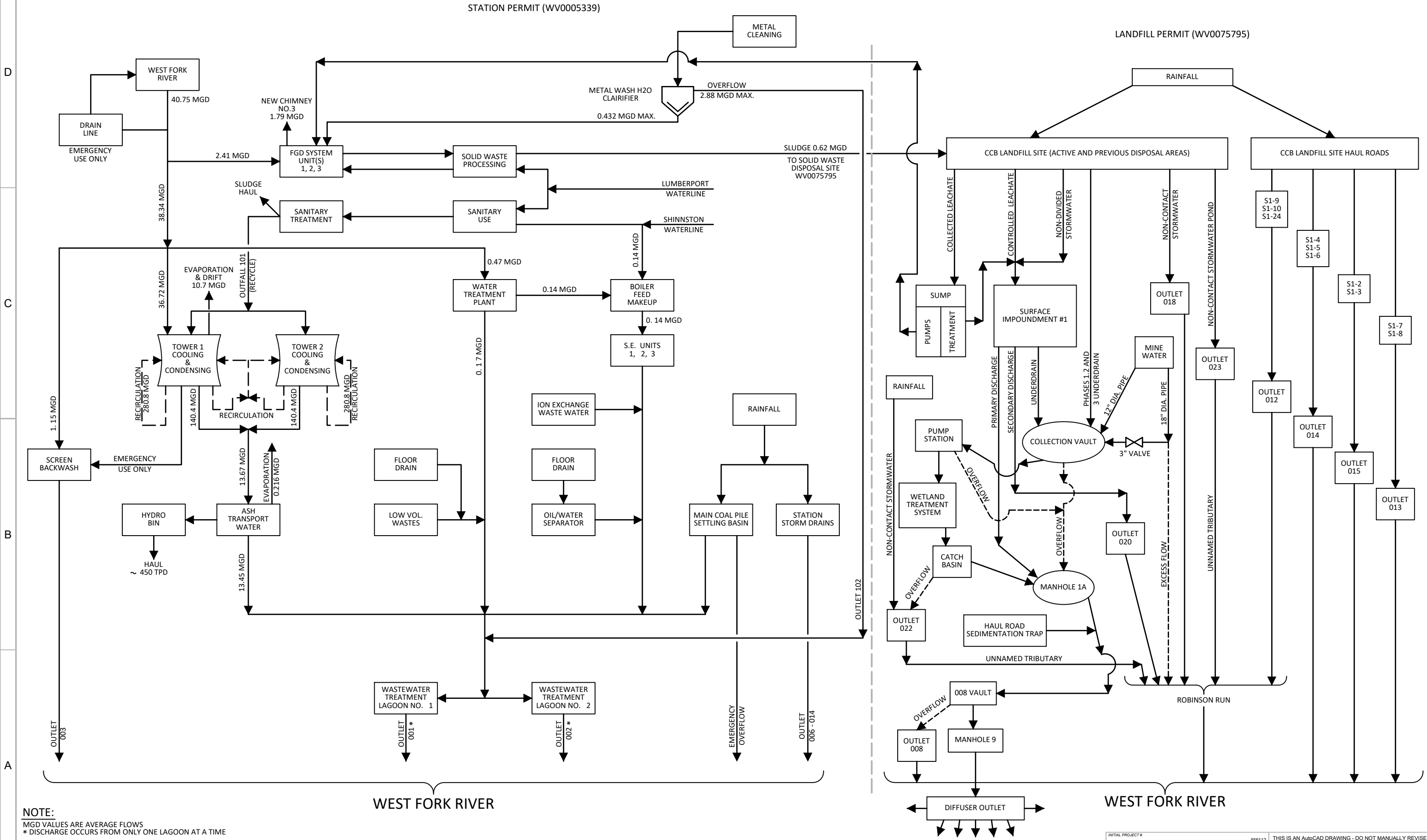
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WATER FLOW LINE DIAGRAM



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Applicant:	MONONGAHELA POWER COMPANY	Type:	Reissue NPDES Industrial
Reference ID:	WV0075795 Harrison P.S. CCR L.F. Renewal (12/04/2020)	Permit ID:	WV0075795
Section XII: Certification			
Status	New	Printed:	Mar. 17, 2021 2:58 PM

**XII. CERTIFICATION (see instructions)**

I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based upon my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

A. NAME Gary J. Dinzeo

OFFICIAL TITLE Director, Harrison Power Station

B. SIGNATURE

C. DATE SIGNED 3/17/2021

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